

**Osnovni podatki o modelu, Vhodni podatki - Konstrukcija**

Datoteka: tower izračun.twp  
Datum preračuna: 10.5.2021

Način preračuna: 3D model

- ☒ Teorija I-ga reda      ☐ Modalna analiza      ☐ Stabilnost  
☐ Teorija II-ga reda      ☐ Seizmični preračun      ☐ Faze gradnje  
☐ Nelinearen preračun

**Velikost modela**

Število vozlišč: 969  
 Število ploskovnih elementov: 775  
 Število grednih elementov: 3  
 Število robnih elementov: 656  
 Število osnovnih obtežnih primerov: 4  
 Število kombinacij obtežb: 26

**Enote mer**

Dolžina: m [cm,mm]  
 Sila: kN  
 Temperatura: Celsius

**Schema nivojev**

Naziv	z [m]	h [m]
plošča	9.55	3.74
pritličje	5.82	5.82

Naziv	z [m]	h [m]
temelj	0.00	

**Tabele materialov**

No	Naziv materiala	E[kN/m <sup>2</sup> ]	$\mu$	$\gamma$ [kN/m <sup>3</sup> ]	$\alpha_t$ [1/C]	Em[kN/m <sup>2</sup> ]	$\mu_m$
1	C 25/30	3.100e+7	0.20	25.00	1.000e-5	3.100e+7	0.20

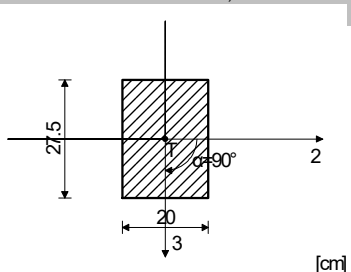
**Seti plošč**

No	d[m]	e[m]	Material	Tip preračuna	Ortotropija	E2[kN/m <sup>2</sup> ]	G[kN/m <sup>2</sup> ]	$\alpha$
<1>	0.360	0.180	1	Tanka plošča	Izotropna			
<2>	0.200	0.100	1	Tanka plošča	Izotropna			

**Seti gred**

Set: 1 Prerez: b/d=20/27.5, Fiktivna ekscentričnost

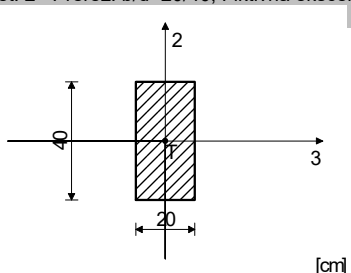
Mat.	A1	A2	A3	I1	I2	I3
1 - C 25/30	5.500e-2	4.583e-2	4.583e-2	4.052e-4	3.466e-4	1.833e-4



[cm]

Set: 2 Prerez: b/d=20/40, Fiktivna ekscentričnost

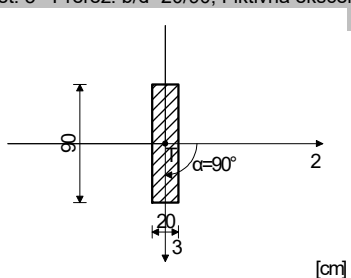
Mat.	A1	A2	A3	I1	I2	I3
1 - C 25/30	8.000e-2	6.667e-2	6.667e-2	7.324e-4	2.667e-4	1.067e-3



[cm]

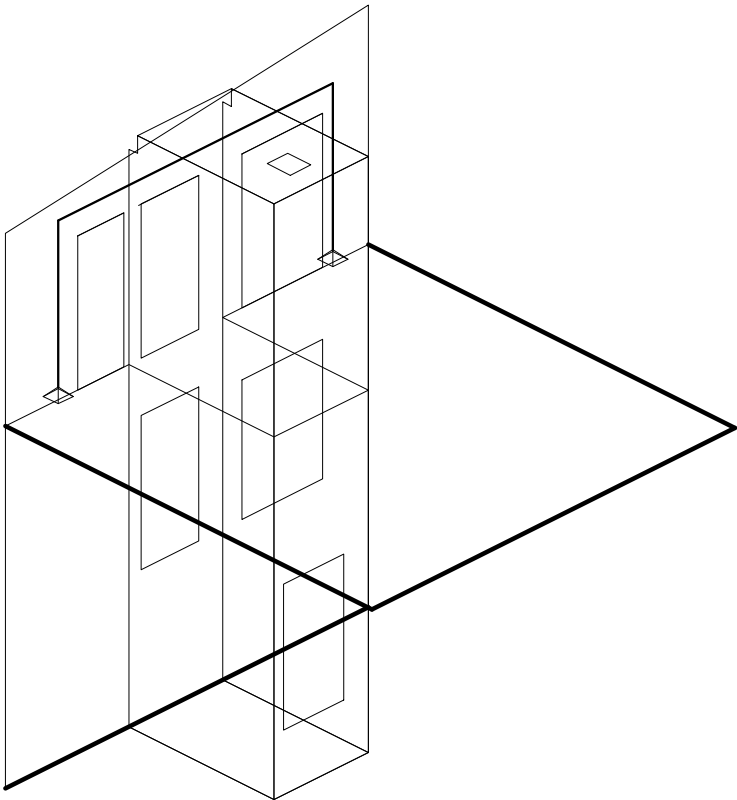
Set: 3 Prerez: b/d=20/90, Fiktivna ekscentričnost

Mat.	A1	A2	A3	I1	I2	I3
1 - C 25/30	1.800e-1	1.500e-1	1.500e-1	2.064e-3	1.215e-2	6.000e-4

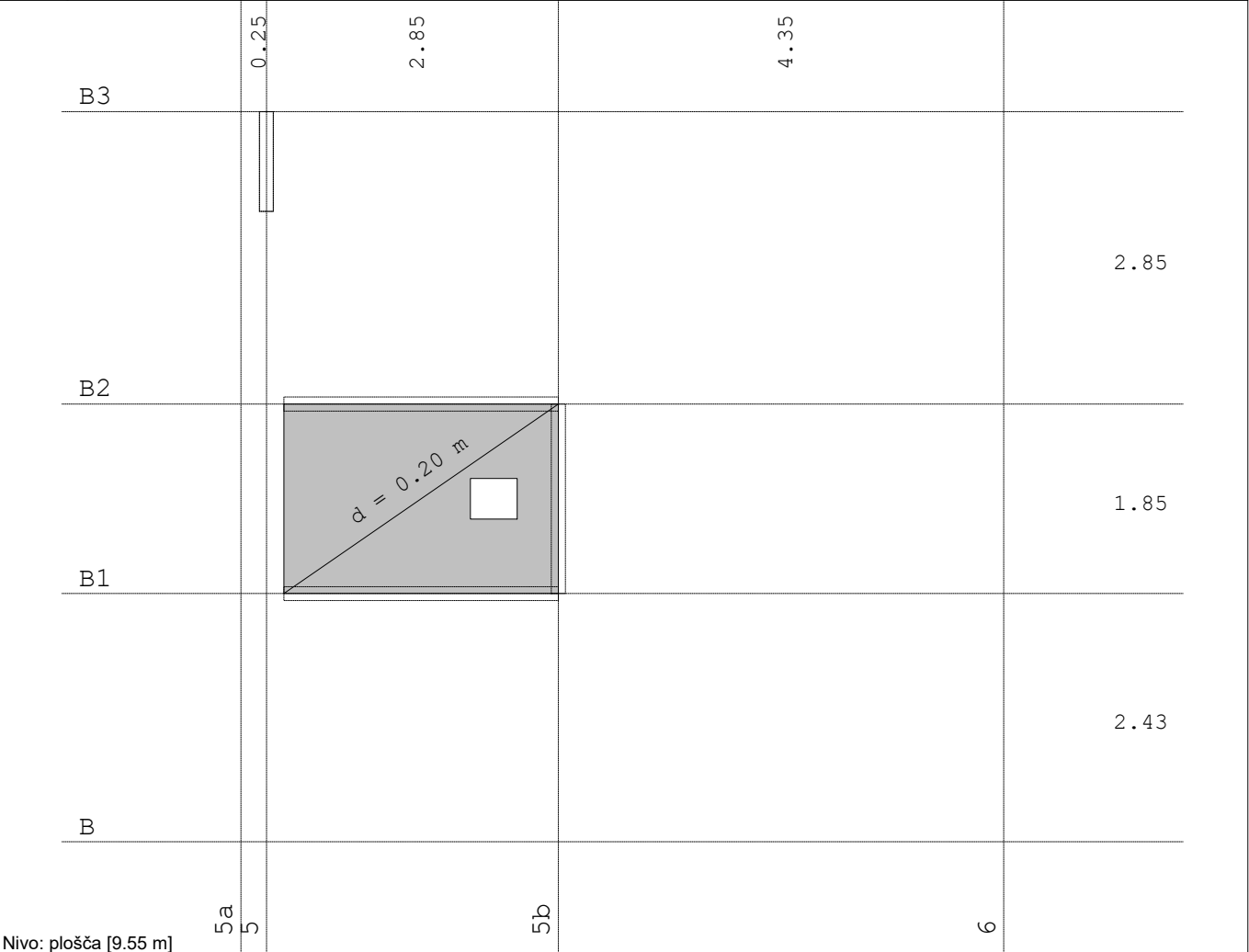


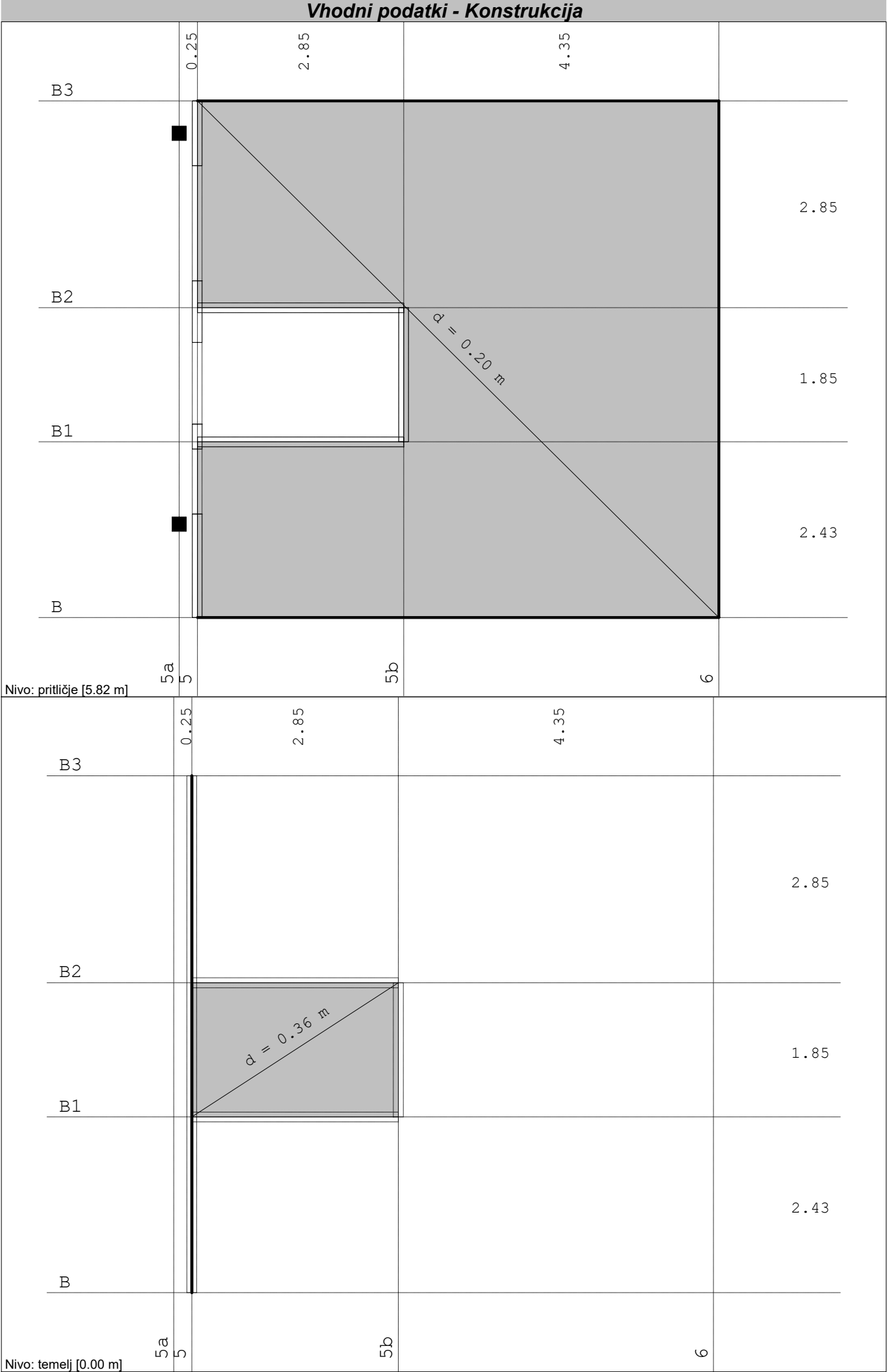
[cm]

Vhodni podatki - Konstrukcija

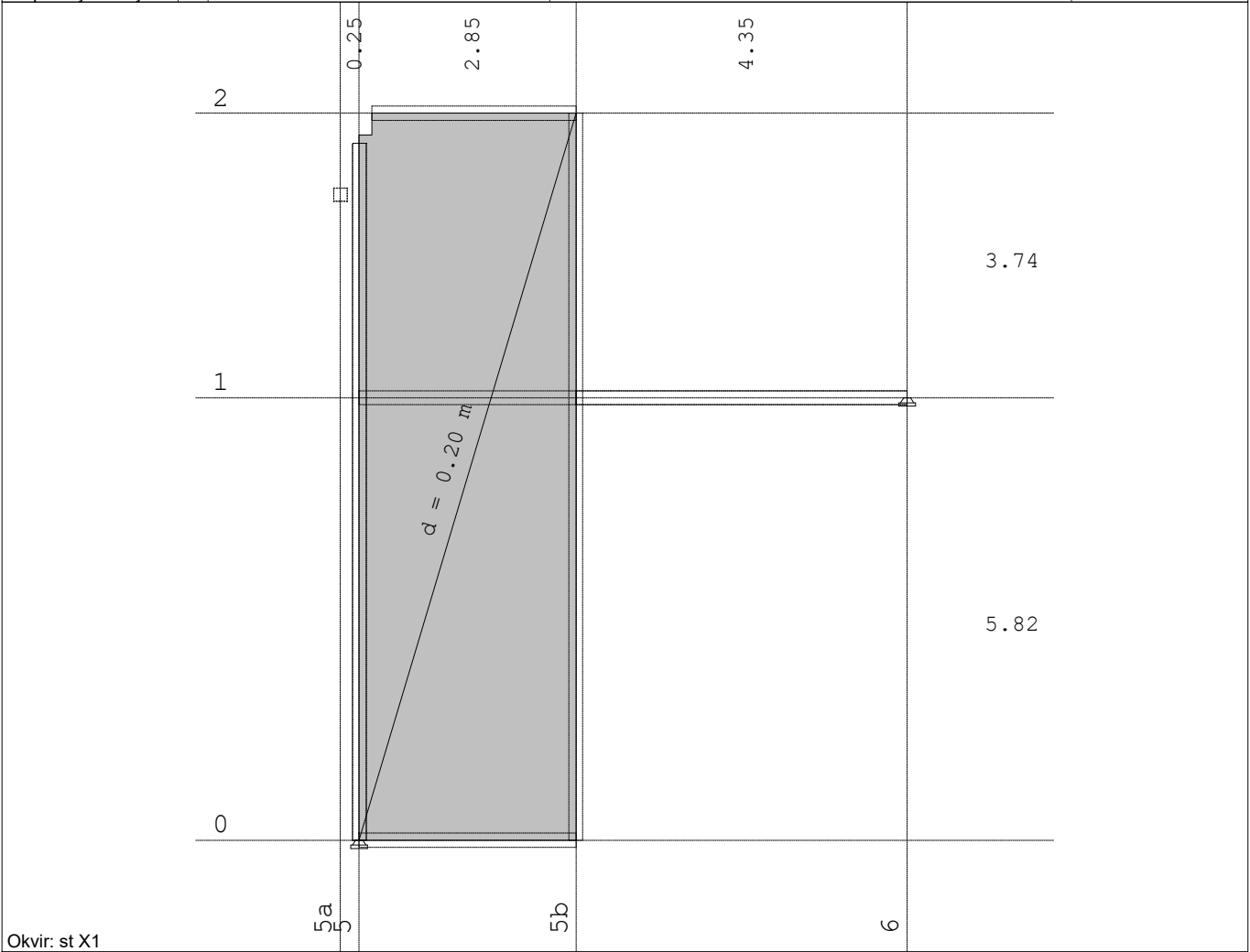


Izometrija

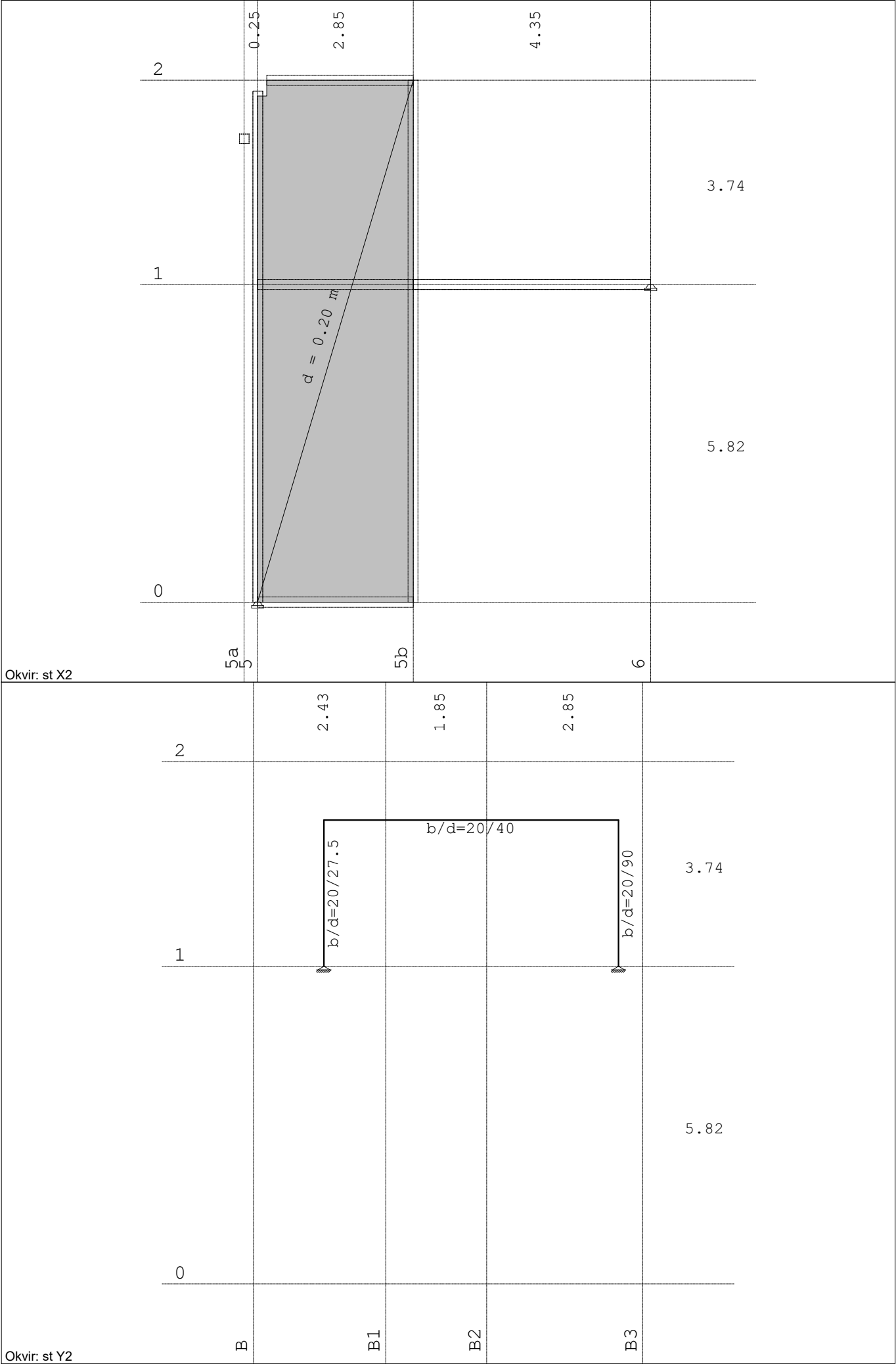




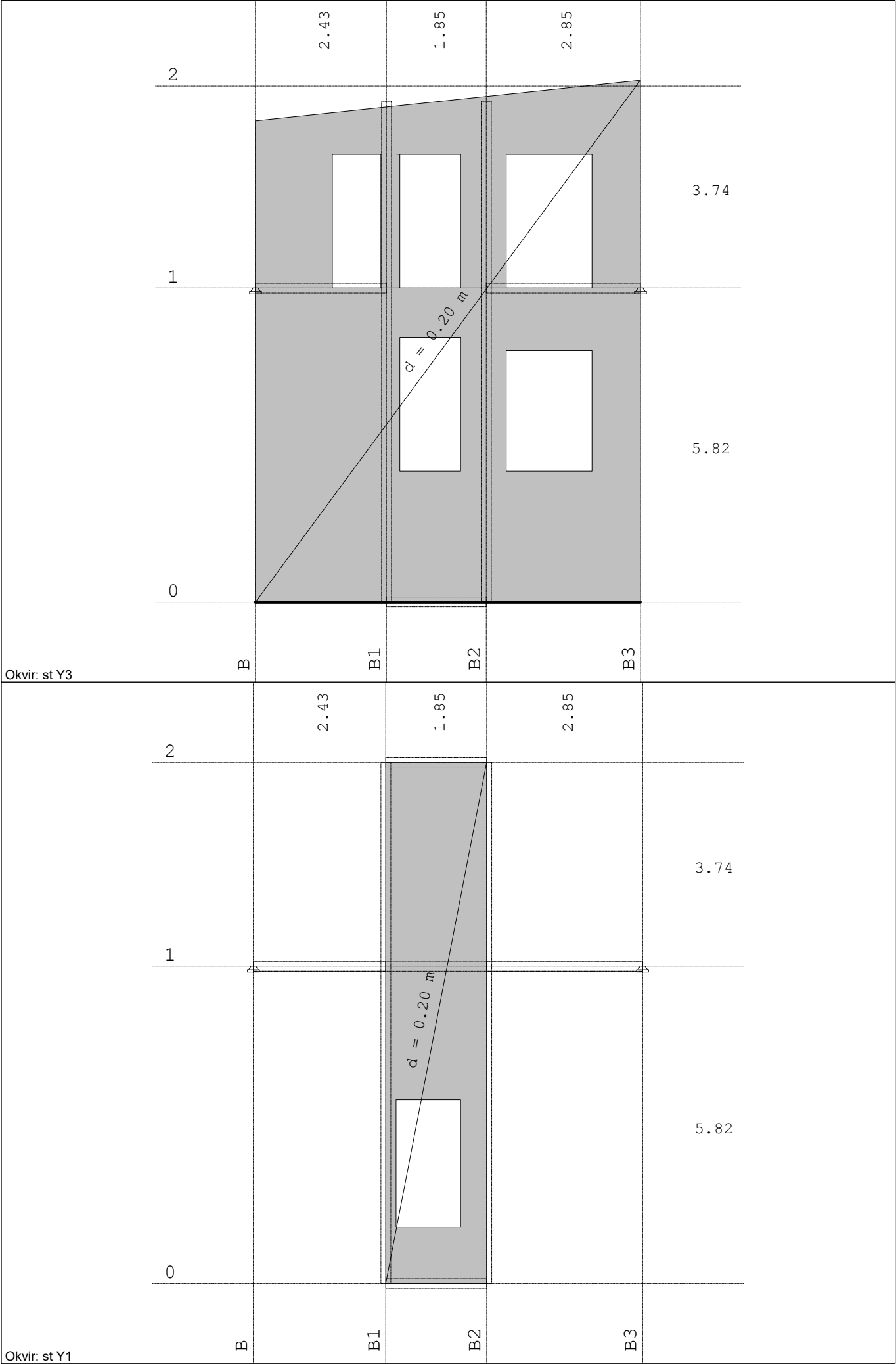
Vhodni podatki - Konstrukcija					
B3	0.25	2.85	4.35		
B2	st Y2 st Y3	st X2			2.85
B1		st X1	st Y1		1.85
B					2.43
5a	5	5b	6		
Dispozicija okvirjev					



Vhodni podatki - Konstrukcija



Vhodni podatki - Konstrukcija



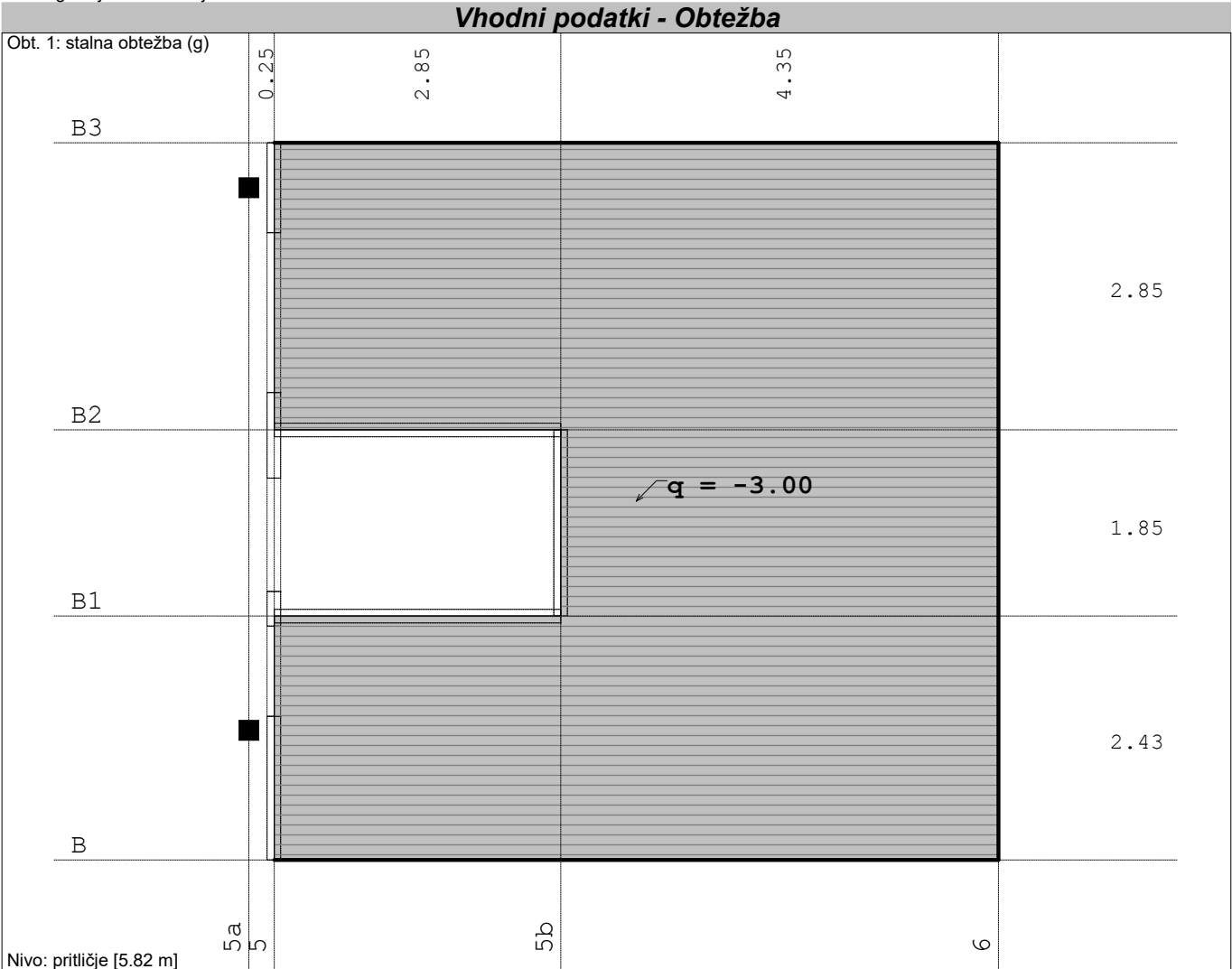
## Vhodni podatki - Obtežba

## Lista obtežnih primerov

LC	Naziv
1	stalna obtežba (g)
2	sneg + veter
3	koristna obtežba plošče pritličja
4	vplivi od dvigala
5	Komb.: 1.35xI+1.5xII+1.05xIII+1.5xIV
6	Komb.: 1.35xI+0.75xII+1.5xIII+1.5xIV
7	Komb.: I+1.5xII+1.05xIII+1.5xIV
8	Komb.: I+0.75xII+1.5xIII+1.5xIV
9	Komb.: 1.35xI+0.75xII+1.05xIII+1.5xIV
10	Komb.: 1.35xI+1.5xIII+1.5xIV
11	Komb.: 1.35xI+1.5xII+1.5xIV
12	Komb.: I+0.75xII+1.05xIII+1.5xIV
13	Komb.: I+1.5xIII+1.5xIV
14	Komb.: I+1.5xII+1.5xIV
15	Komb.: 1.35xI+1.05xIII+1.5xIV
16	Komb.: 1.35xI+1.5xII+1.05xIII
17	Komb.: 1.35xI+0.75xII+1.5xIV
18	Komb.: 1.35xI+0.75xII+1.5xIII
19	Komb.: I+1.05xIII+1.5xIV
20	Komb.: I+1.5xII+1.05xIII
21	Komb.: I+0.75xII+1.5xIV
22	Komb.: I+0.75xII+1.5xIII
23	Komb.: 1.35xI+1.5xIV
24	Komb.: 1.35xI+1.5xIII
25	Komb.: 1.35xI+1.5xII
26	Komb.: I+1.5xIV
27	Komb.: I+1.5xIII
28	Komb.: I+1.5xII
29	Komb.: 1.35xI
30	Komb.: I

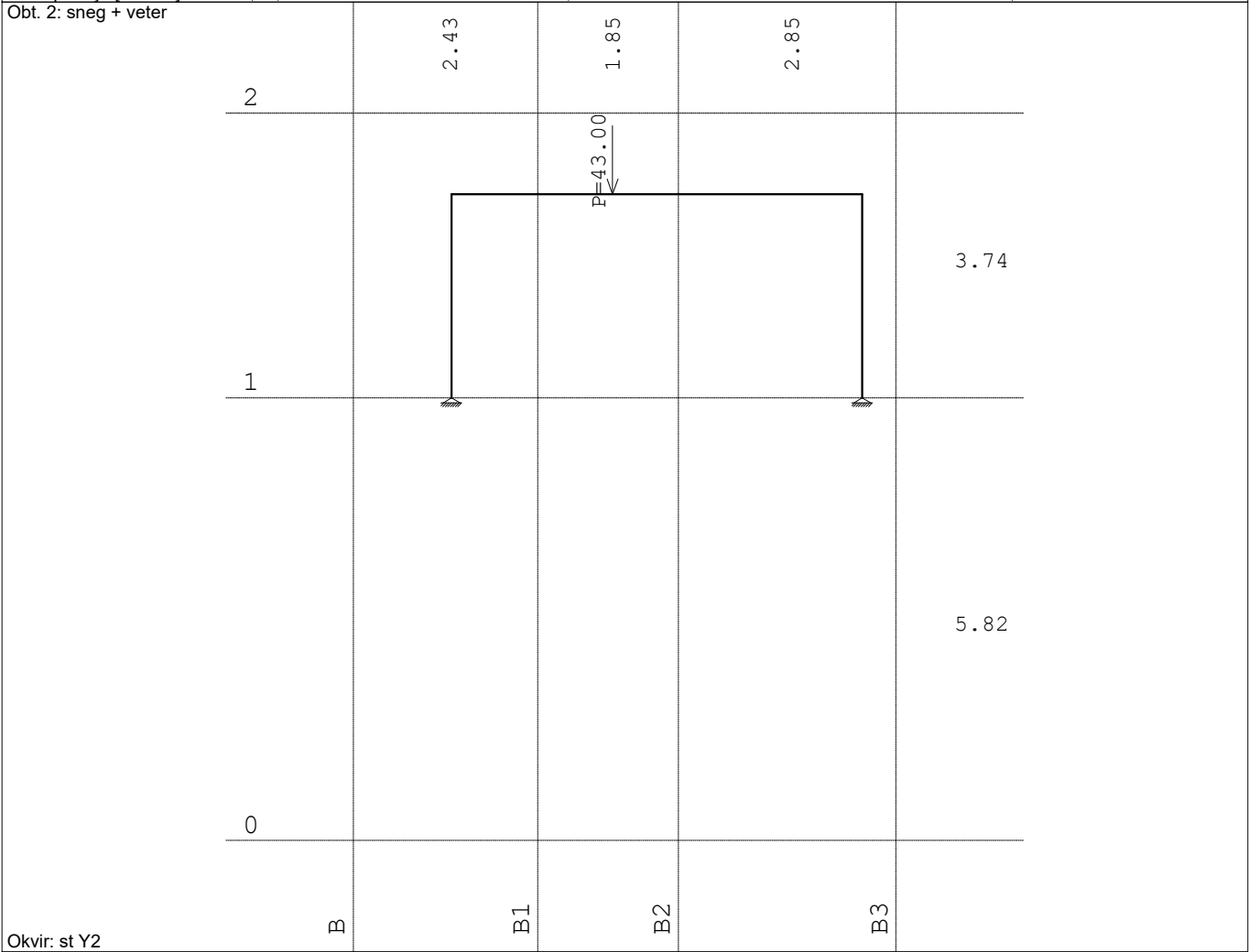
Obt. 1: stalna obtežba (g)

	0.25	2.85	4.35	
B3				
				2.85
B2				
				1.85
B1				
				2.43
B				
	5a	5b	6	
Nivo: plošča [9.55 m]	5			



Nivo: pritličje [5.82 m]

Obt. 2: sneg + veter

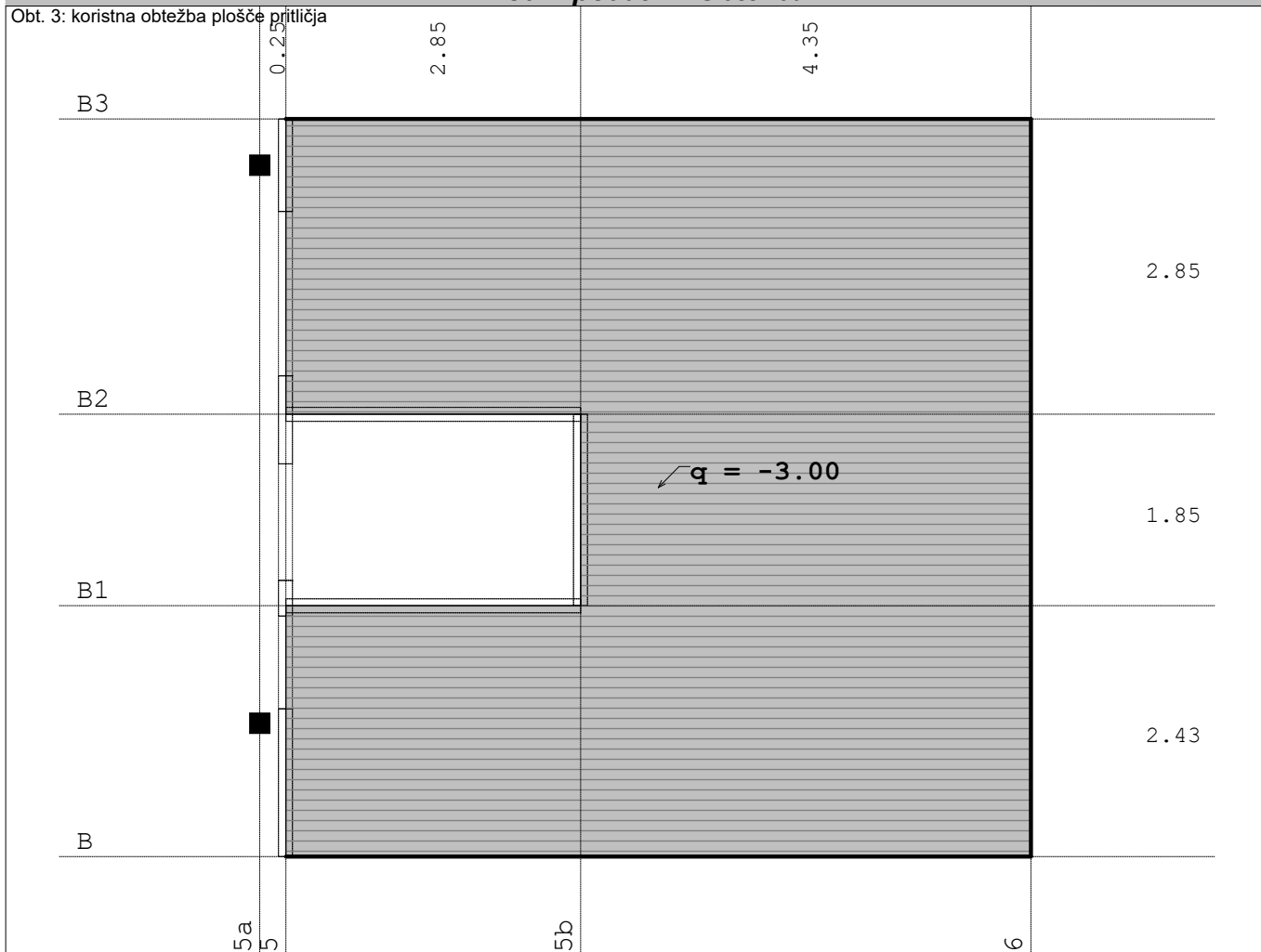


Okvir: st Y2



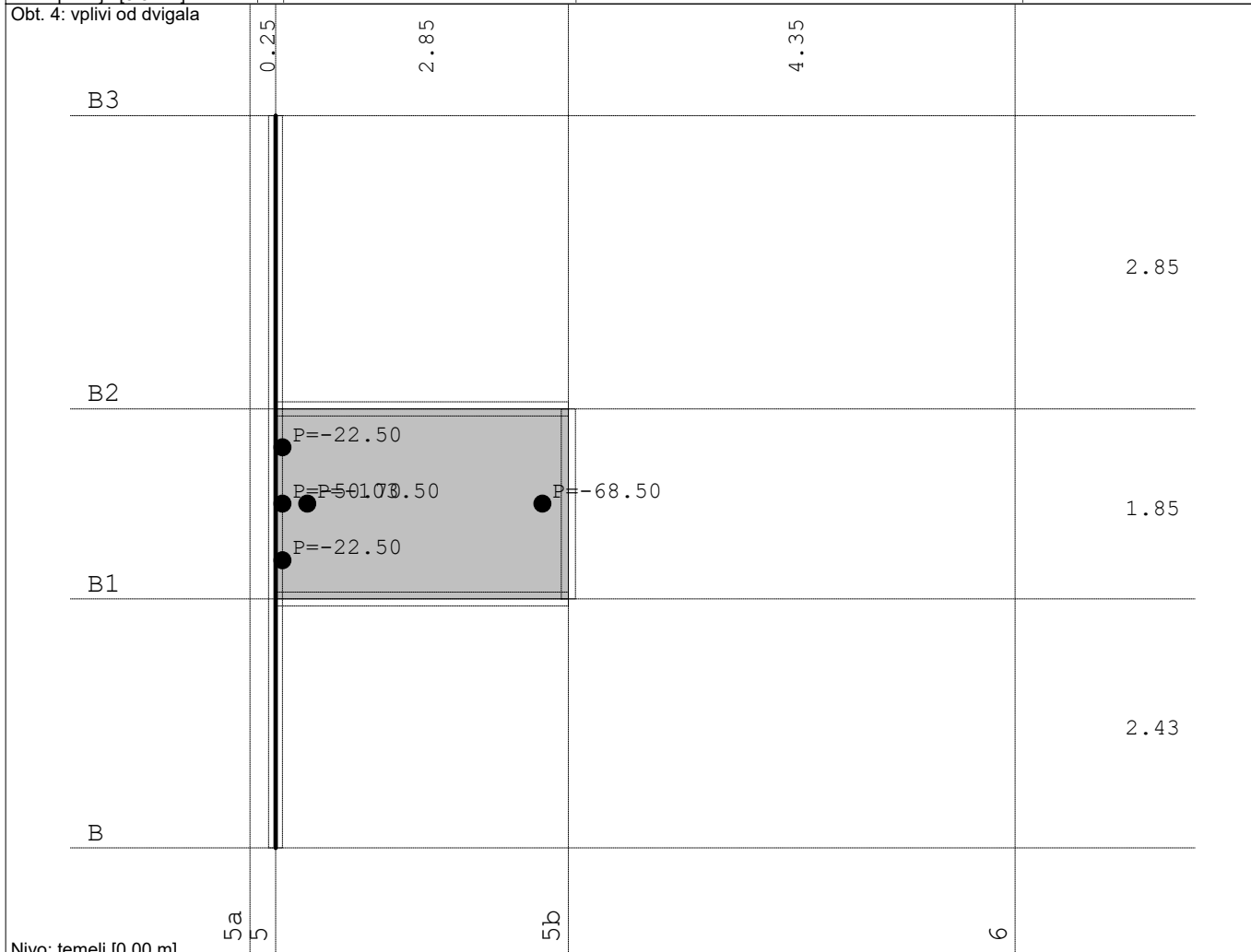
**Vhodni podatki - Obtežba**

Obt. 3: koristna obtežba plošče pritličja



Nivo: pritličje [5.82 m]

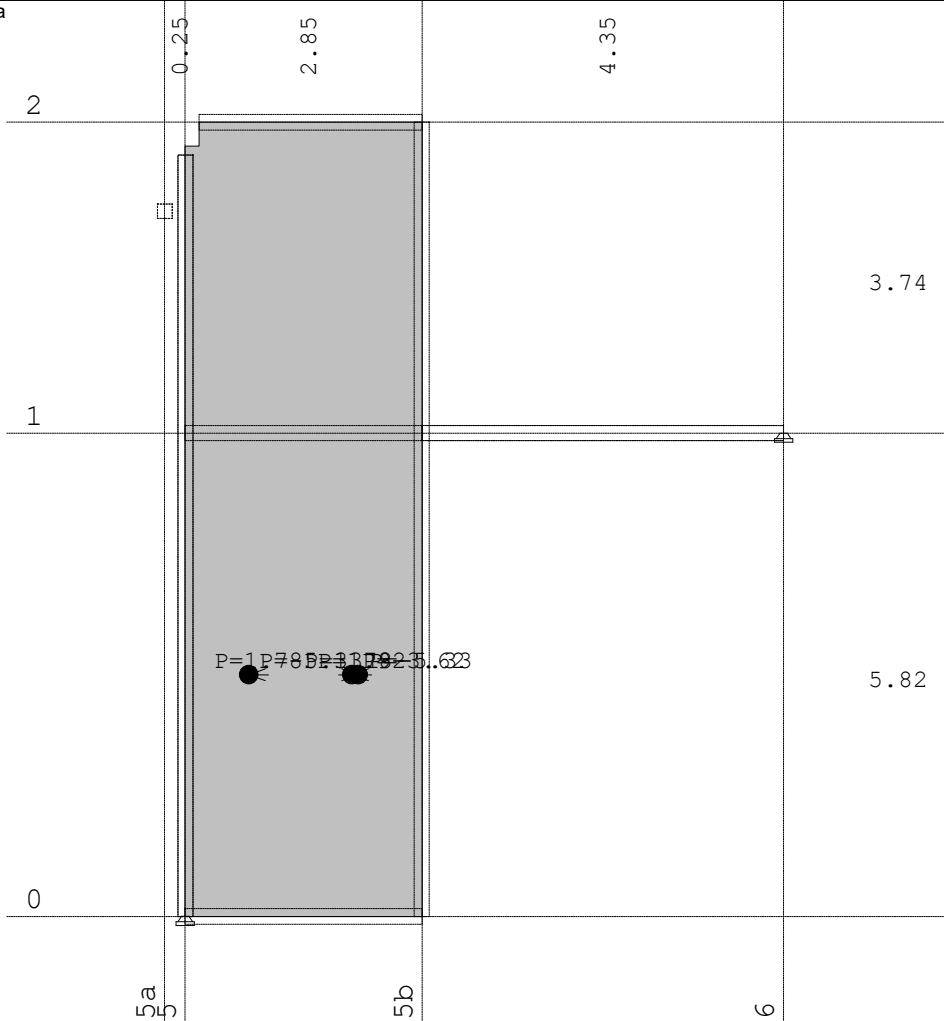
Obt. 4: vplivi od dvigala



Nivo: temelj [0.00 m]

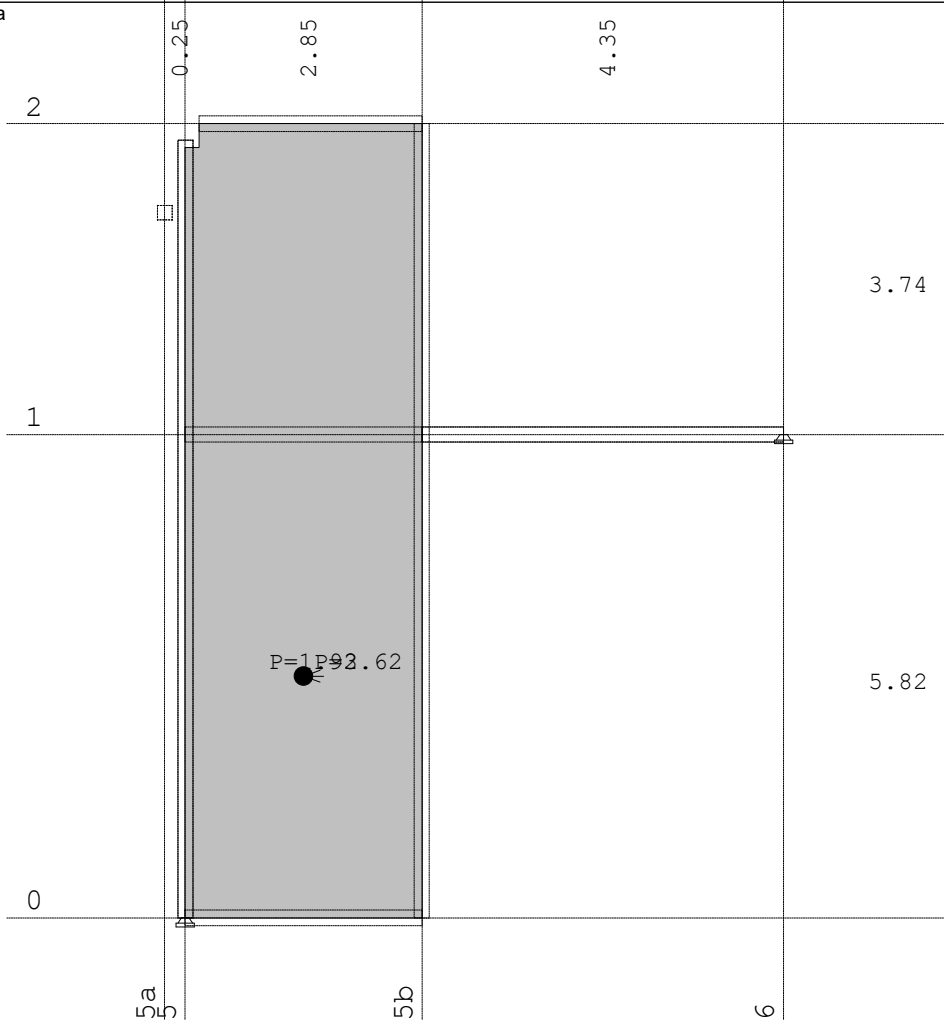
Vhodni podatki - Obtežba

Obt. 4: vplivi od dvigala



Okvir: st X1

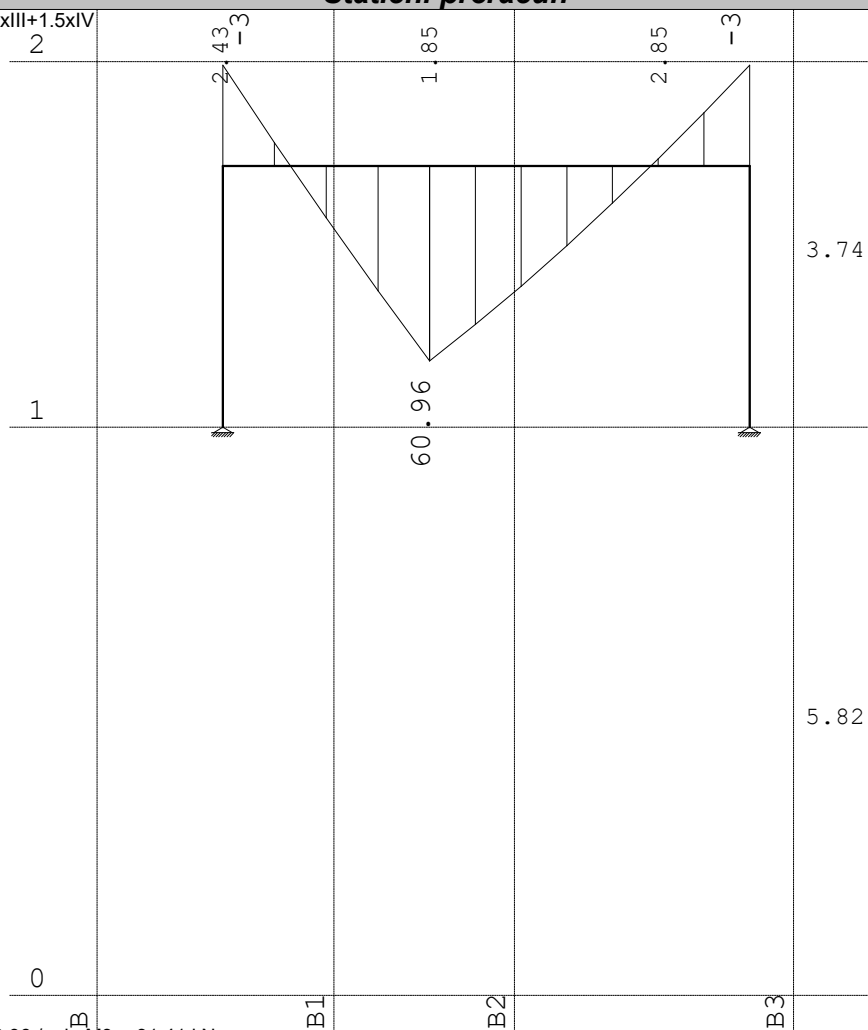
Obt. 4: vplivi od dvigala



Okvir: st X2

## Statični preračun

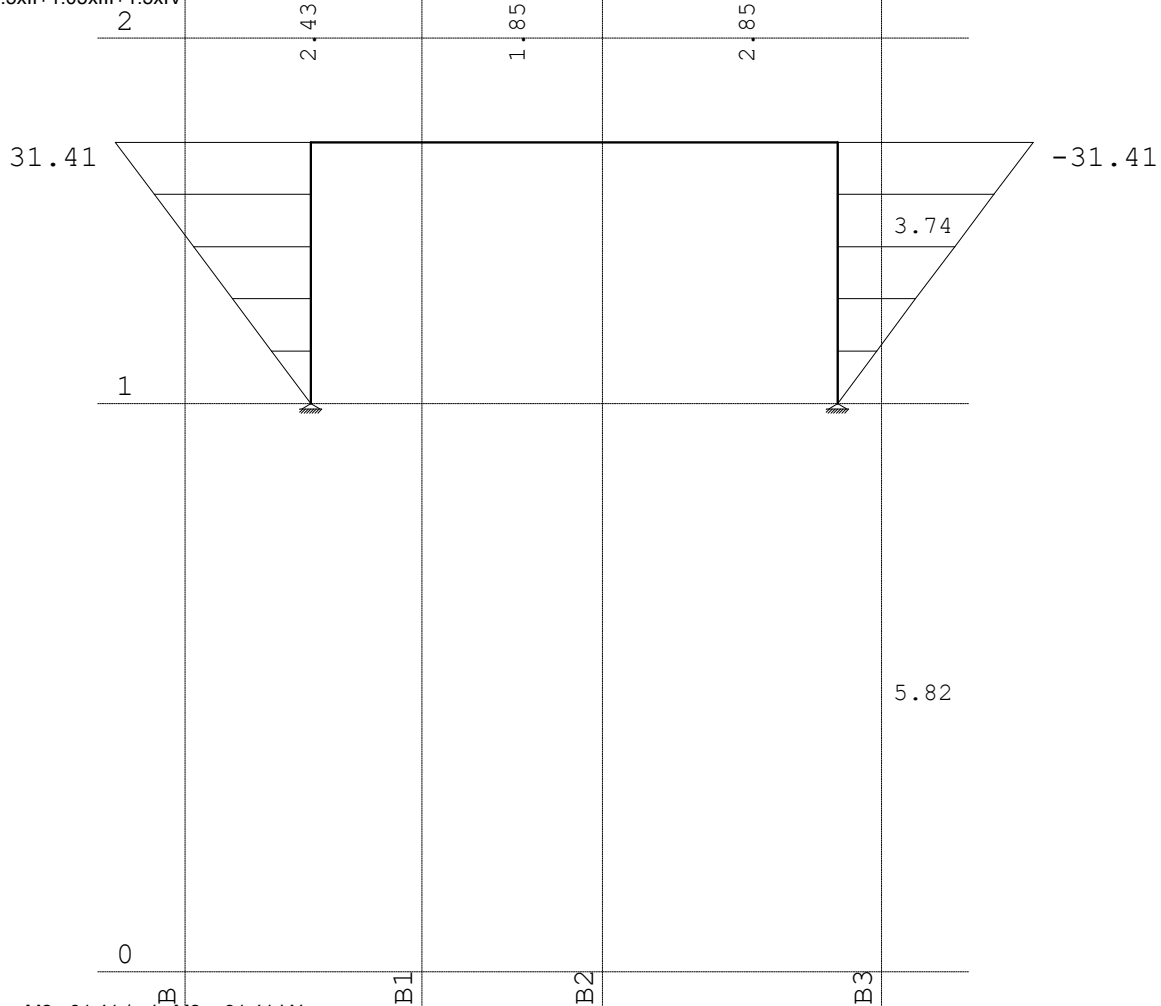
Obt. 5: 1.35xI+1.5xII+1.05xIII+1.5xIV



Okvir: st Y2

Vplivi v gredi: max M3= 60.96 / min M3= -31.41 kNm


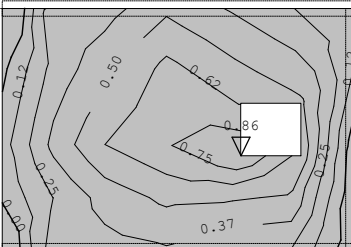

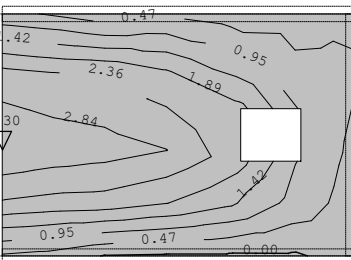
Obt. 5: 1.35xI+1.5xII+1.05xIII+1.5xIV



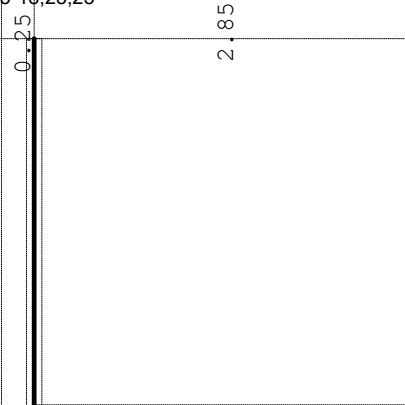
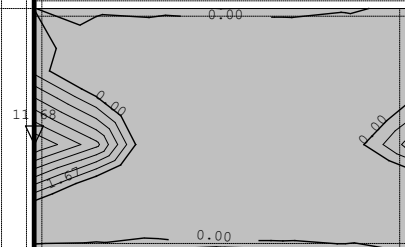
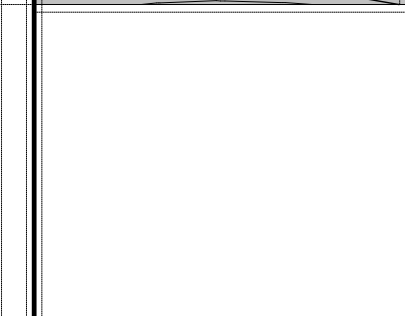
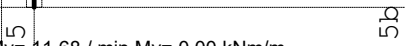
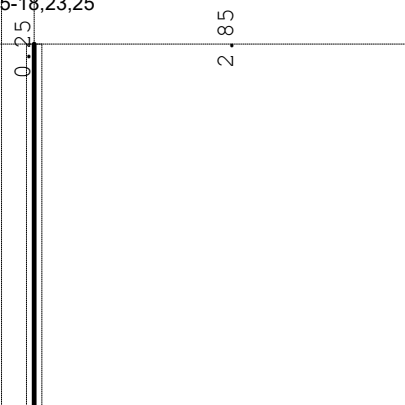
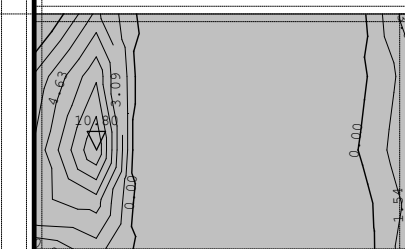
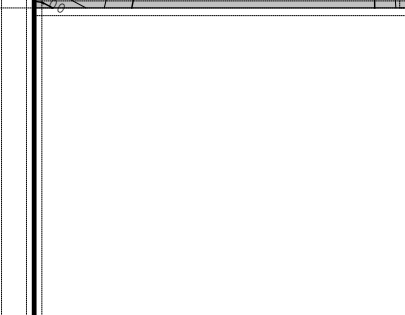
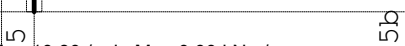
Okvir: st Y2

Vplivi v gredi: max M2= 31.41 / min M2= -31.41 kNm

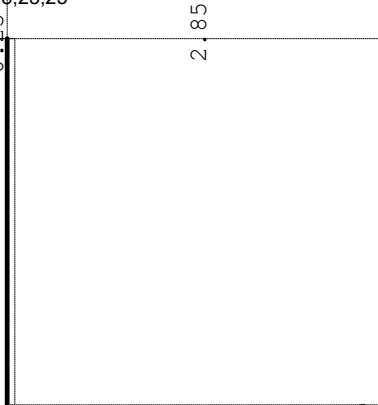
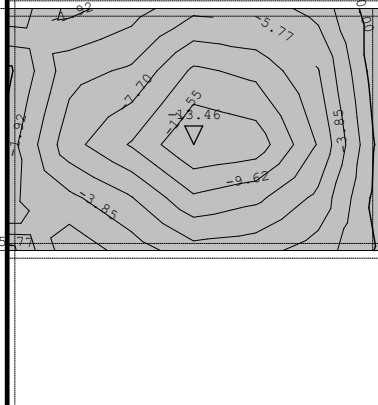
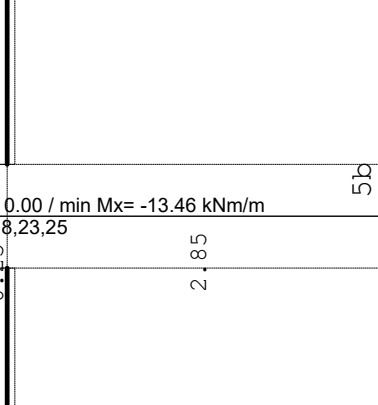
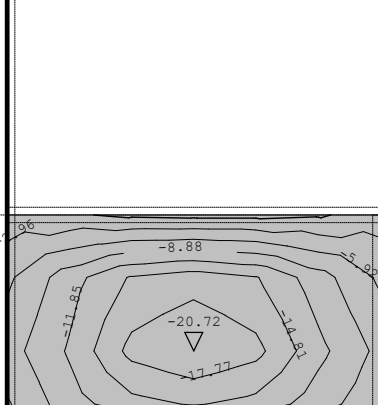
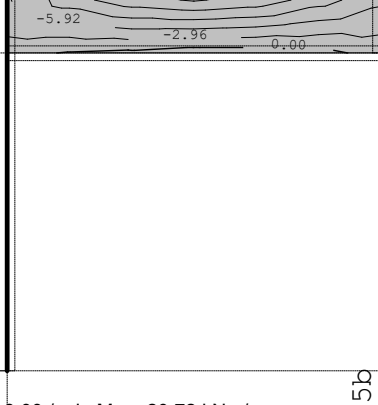
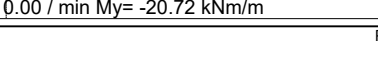
## Statični preračun

Obt. 31: [Ovo] 5-11,15-18,23,25			
B3		4.35	
B2			2.85
B1			1.85
B			2.43
Nivo: plošča [9.55,6] Vplivi v plošči: max Mx= 0.86 / min Mx= 0.00 kNm/m		5b	6
Obt. 31: [Ovo] 5-11,15-18,23,25			
B3		4.35	
B2			2.85
B1			1.85
B			2.43
Nivo: plošča [9.55,6] Vplivi v plošči: max My= 3.30 / min My= 0.00 kNm/m		5b	6

## Statični preračun

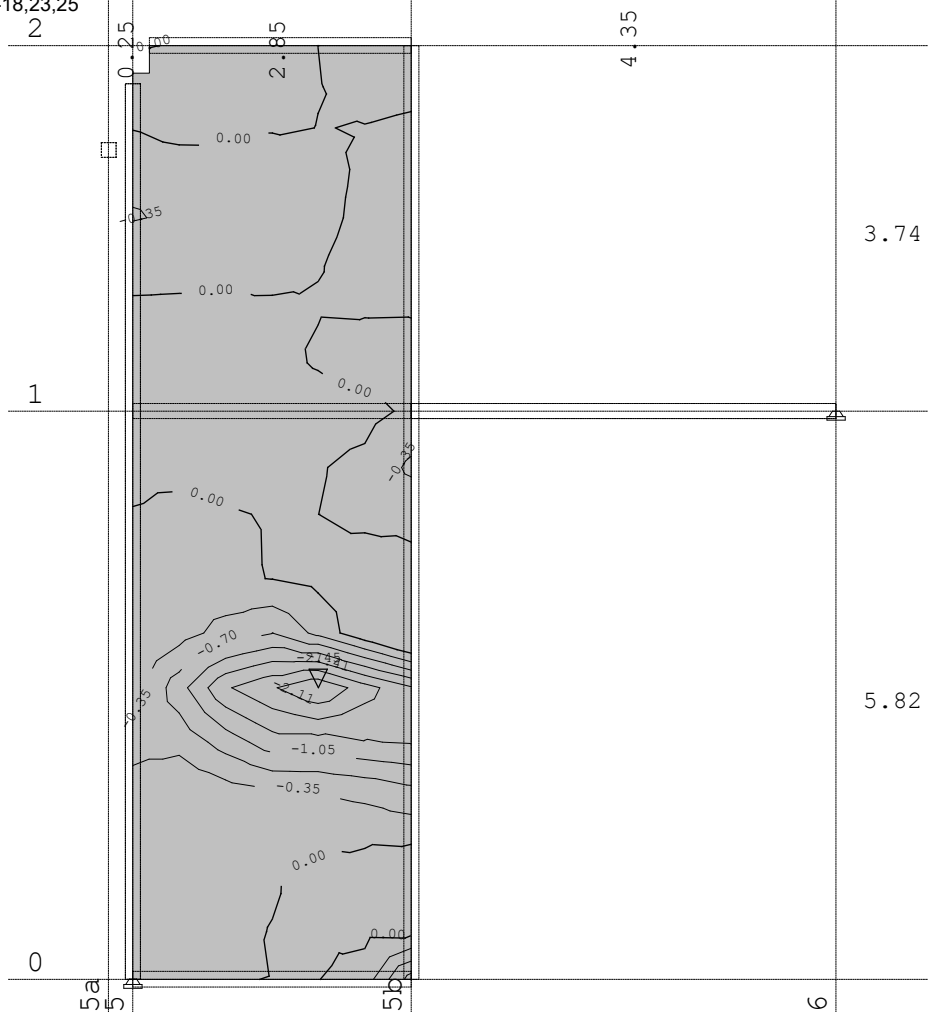
Obt. 31: [Ovo] 5-11,15-18,23,25			
B3		2.85	4.35
B2		1.85	
B1		2.43	
B		6	
Nivo: temelj [0.00 m] Vplivi v plošči: max My= 11.68 / min My= 0.00 kNm/m			
Obt. 31: [Ovo] 5-11,15-18,23,25			
B3		2.85	4.35
B2		1.85	
B1		2.43	
B		6	
Nivo: temelj [0.00 m] Vplivi v plošči: max Mx= 10.80 / min Mx= 0.00 kNm/m			

## Statični preračun

Obt. 31: [Ovo] 5-11,15-18,23,25			
B3		2.85	
B2		1.85	
B1		2.43	
B			
Nivo: temelj [0.00 m] Vplivi v plošči: max Mx= 0.00 / min Mx= -13.46 kNm/m			
Obt. 31: [Ovo] 5-11,15-18,23,25			
B3		2.85	
B2		1.85	
B1		2.43	
B			
Nivo: temelj [0.00 m] Vplivi v plošči: max My= 0.00 / min My= -20.72 kNm/m			

## Statični preračun

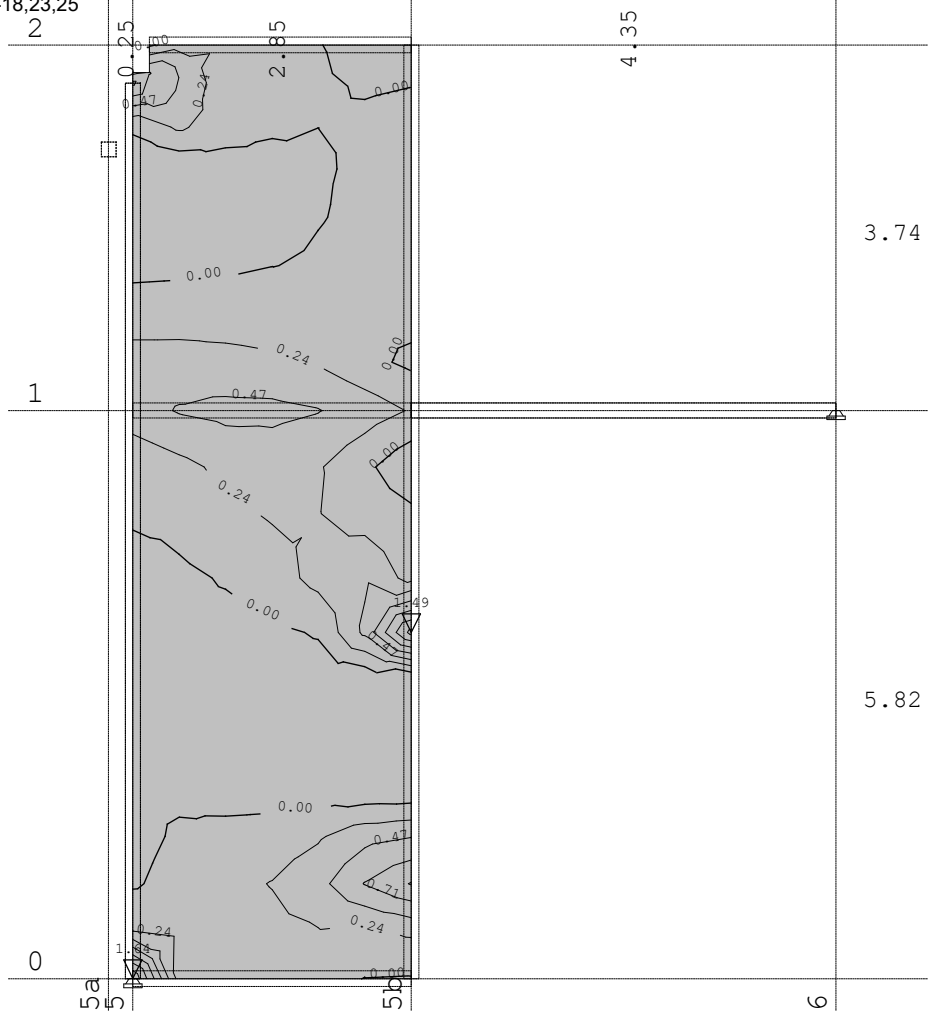
Obt. 31: [Ovo] 5-11,15-18,23,25



Okvir: st X1

Vplivi v plošči: max  $M_y = 0.00$  / min  $M_y = -2.45$  kNm/m

Obt. 31: [Ovo] 5-11,15-18,23,25

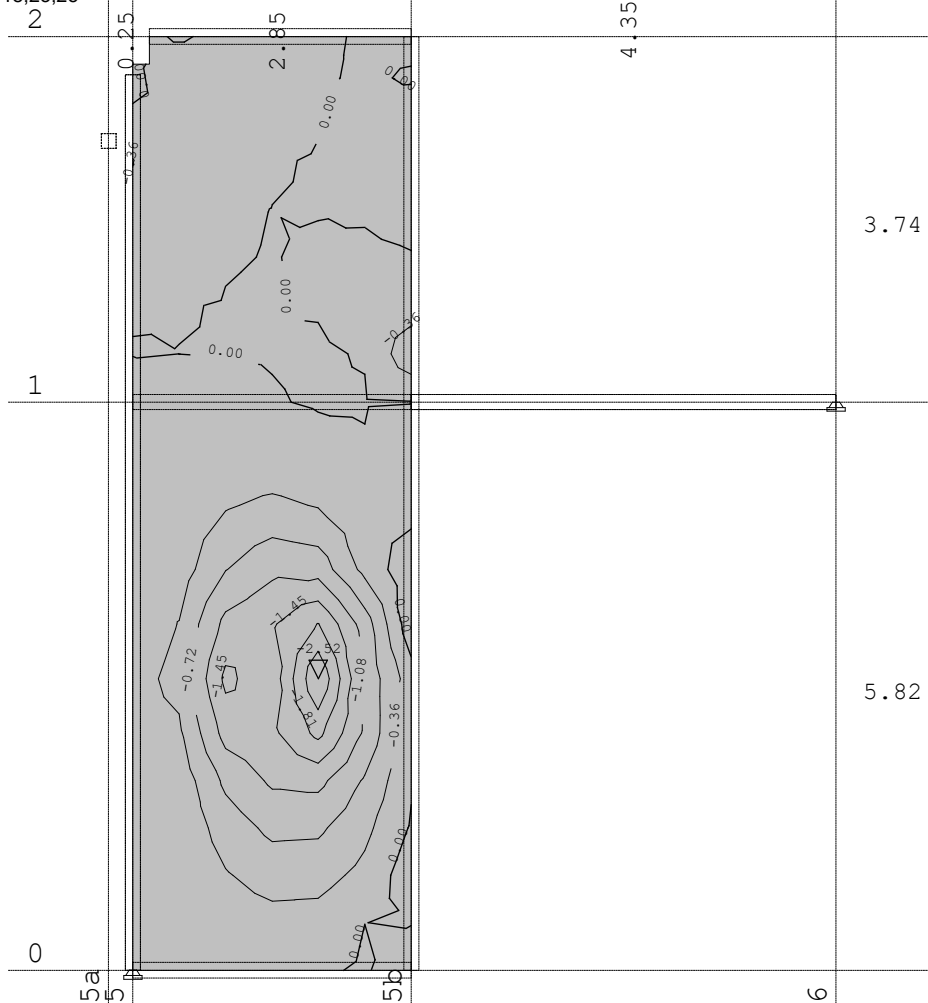


Okvir: st X1

Vplivi v plošči: max  $M_y = 1.64$  / min  $M_y = 0.00$  kNm/m

## Statični preračun

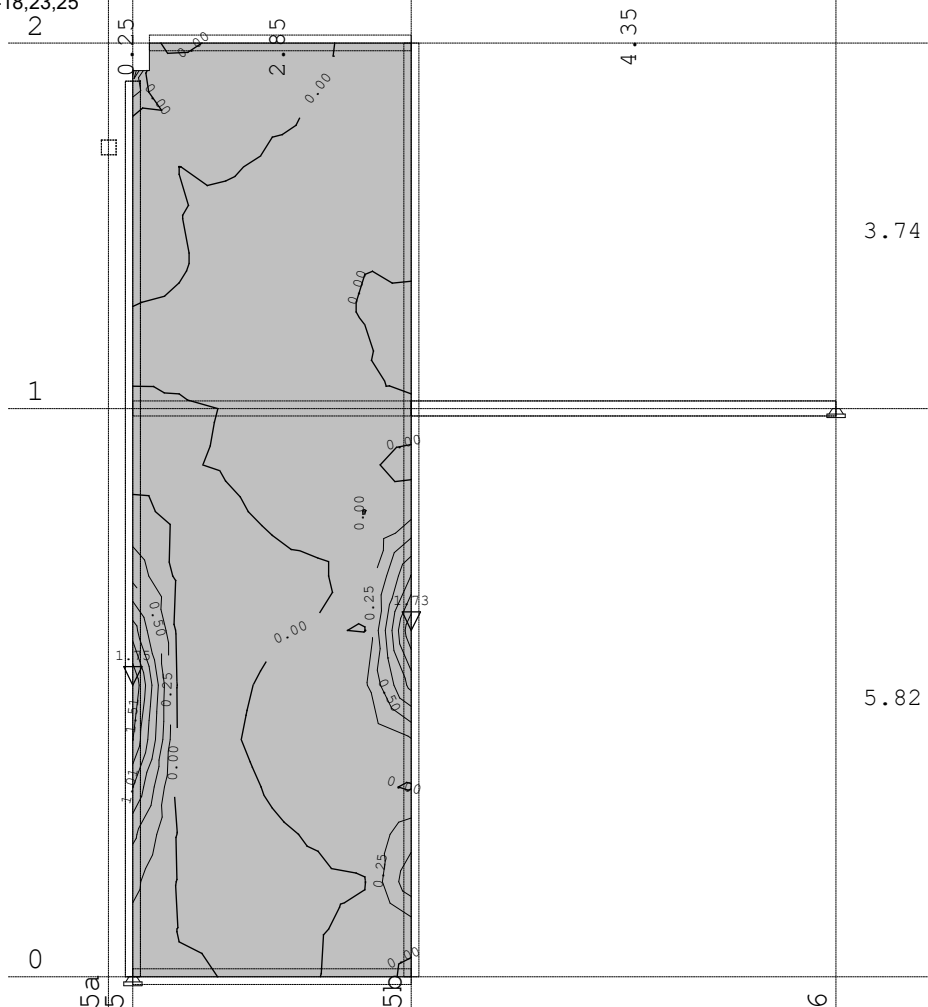
Obt. 31: [Ovo] 5-11,15-18,23,25



Okvir: st X1

Vplivi v plošči: max  $M_x = 0.00$  / min  $M_x = -2.52$  kNm/m

Obt. 31: [Ovo] 5-11,15-18,23,25



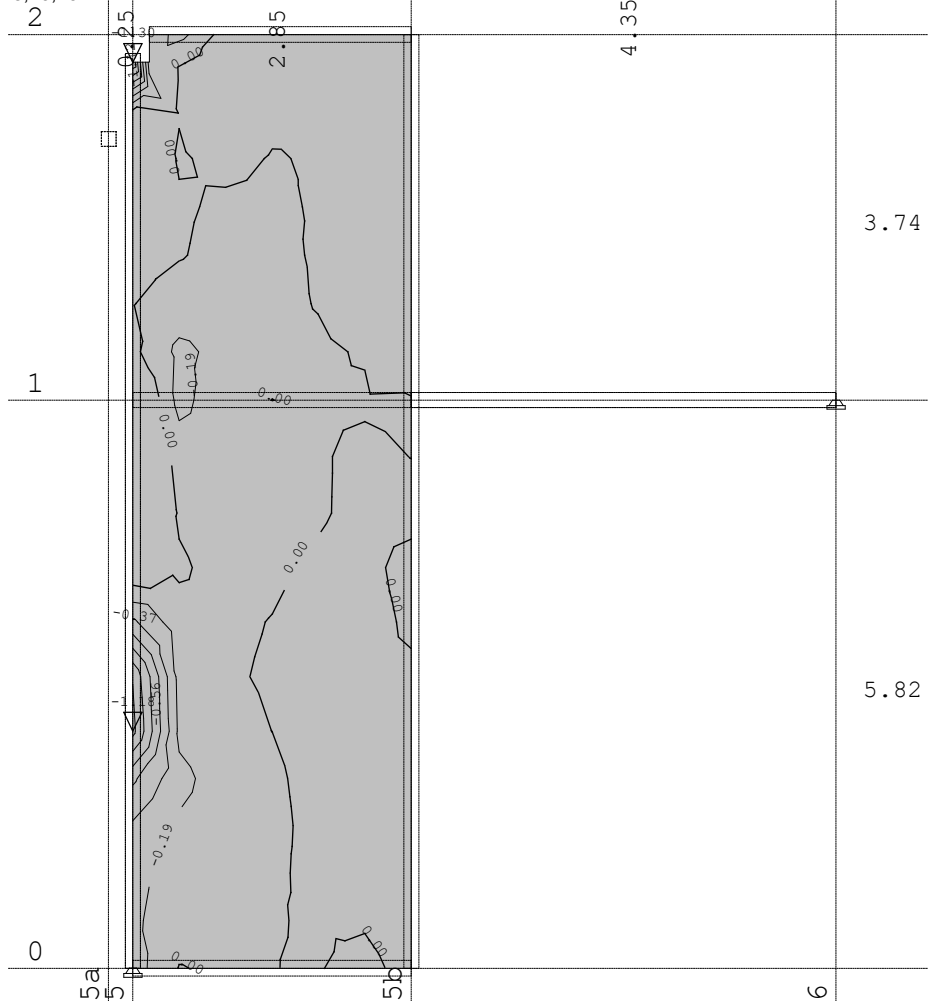
Okvir: st X1

Vplivi v plošči: max  $M_x = 1.75$  / min  $M_x = 0.00$  kNm/m



## Statični preračun

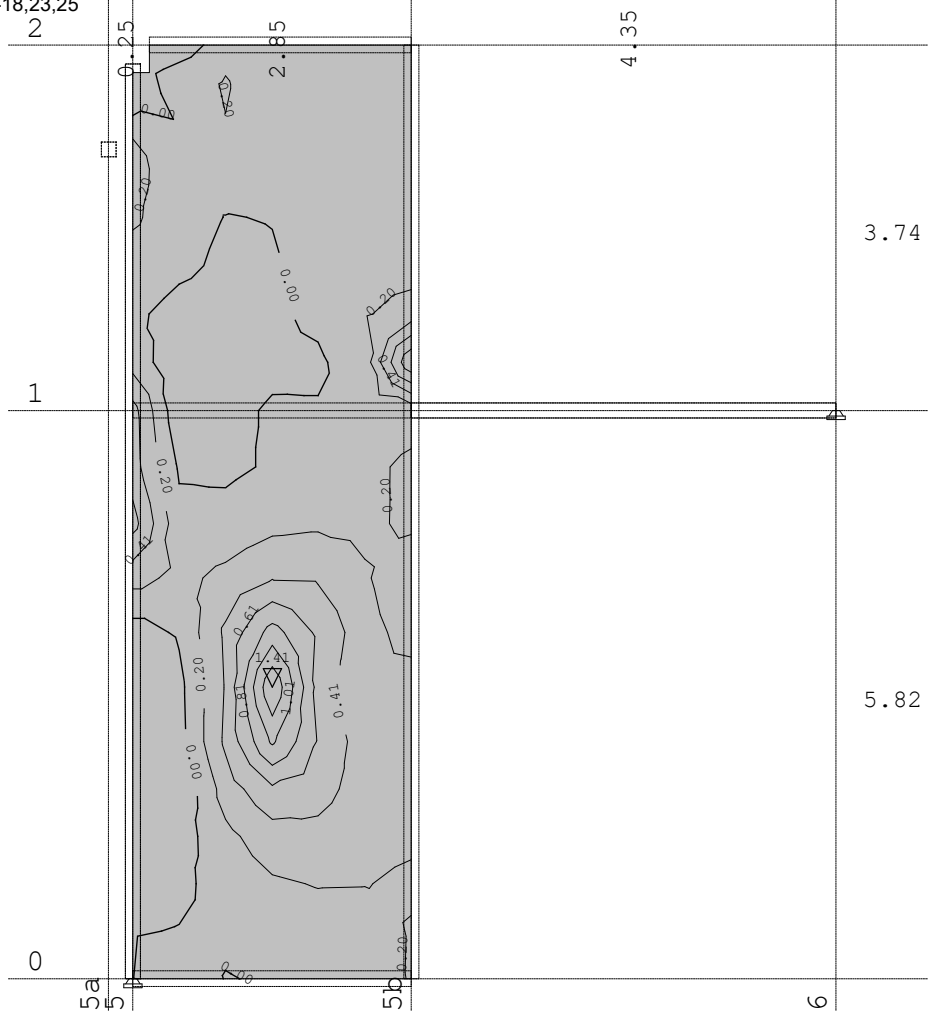
Obt. 31: [Ovo] 5-11,15-18,23,25



Okvir: st X2

Vplivi v plošči: max  $M_x = 0.00$  / min  $M_x = -1.30$  kNm/m

Obt. 31: [Ovo] 5-11,15-18,23,25



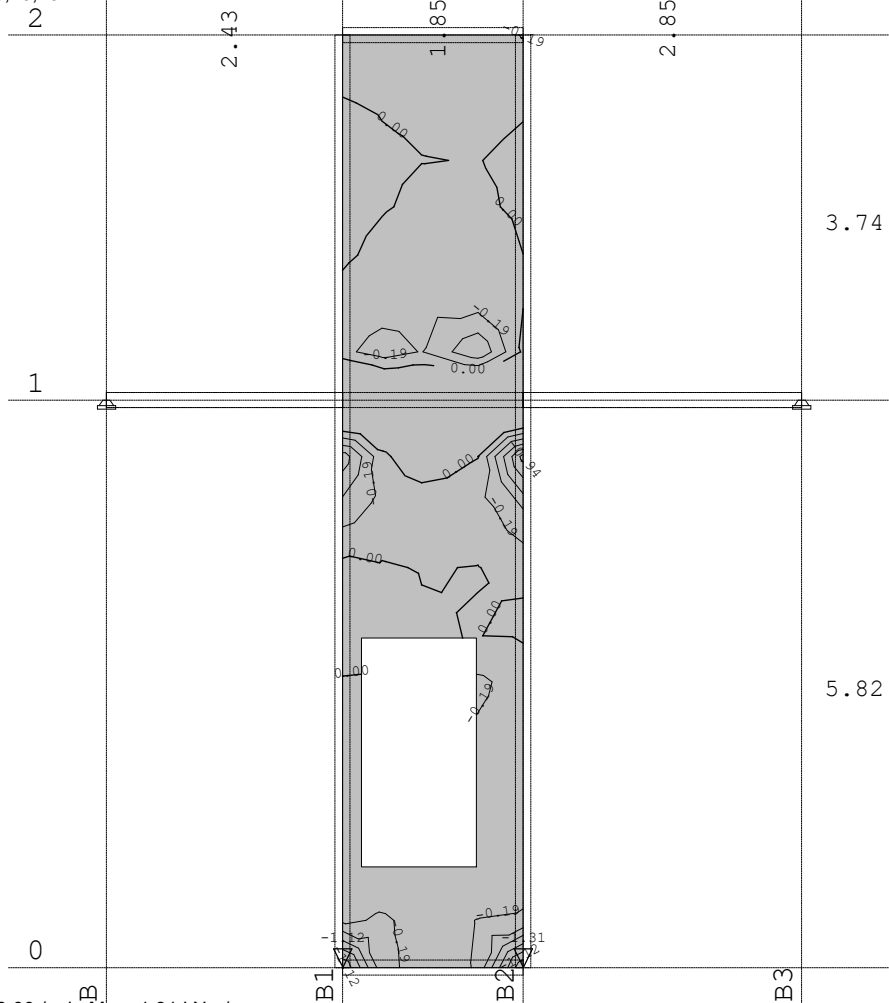
Okvir: st X2

Vplivi v plošči: max  $M_x = 1.41$  / min  $M_x = 0.00$  kNm/m

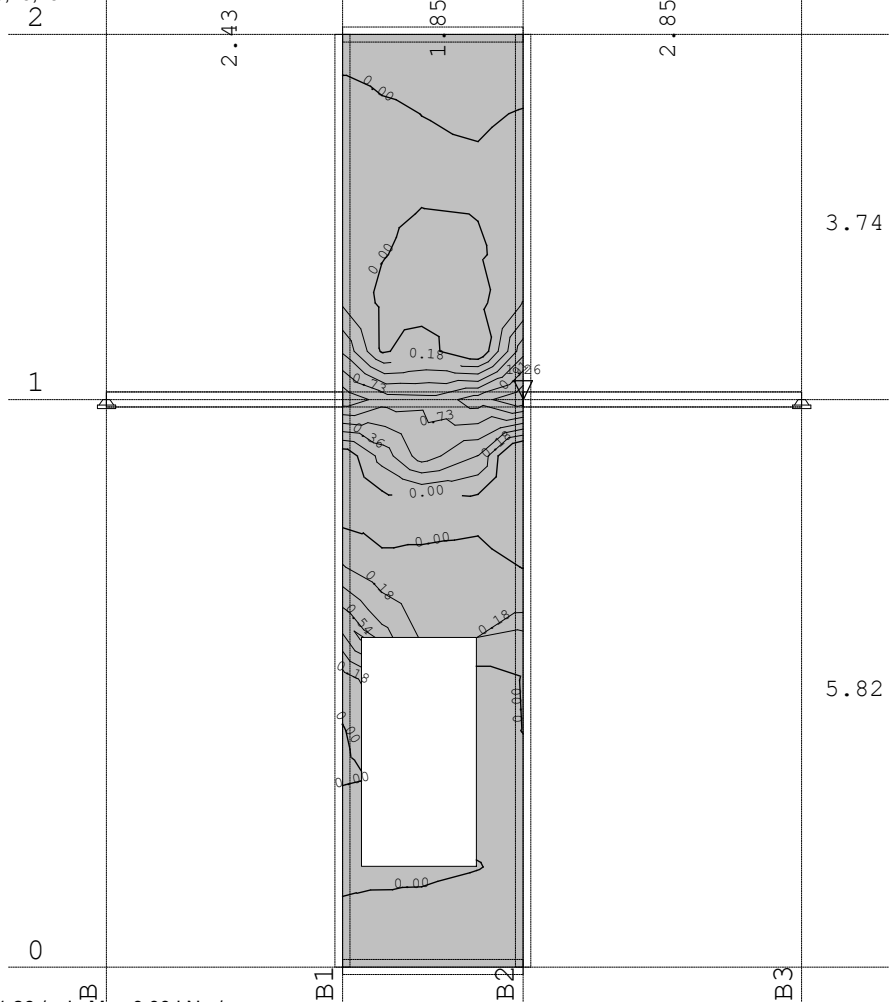


## Statični preračun

Obt. 31: [Ovo] 5-11,15-18,23,25

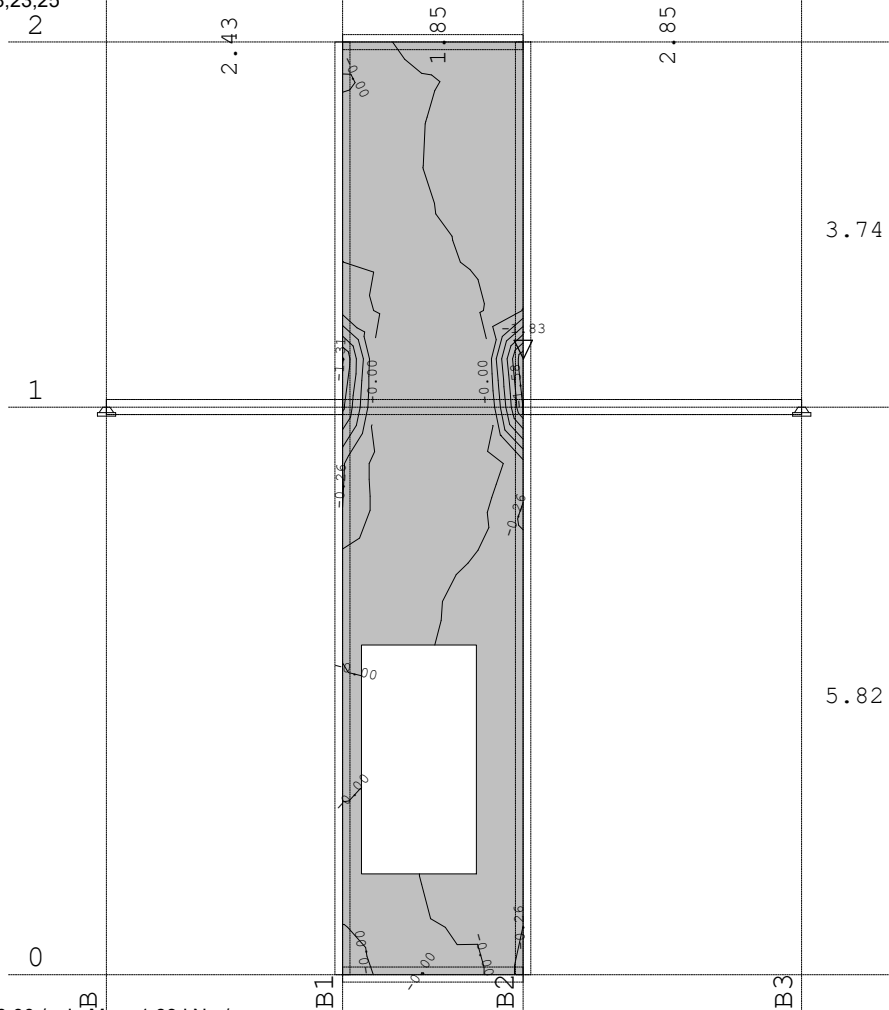


Obt. 31: [Ovo] 5-11,15-18,23,25



## Statični preračun

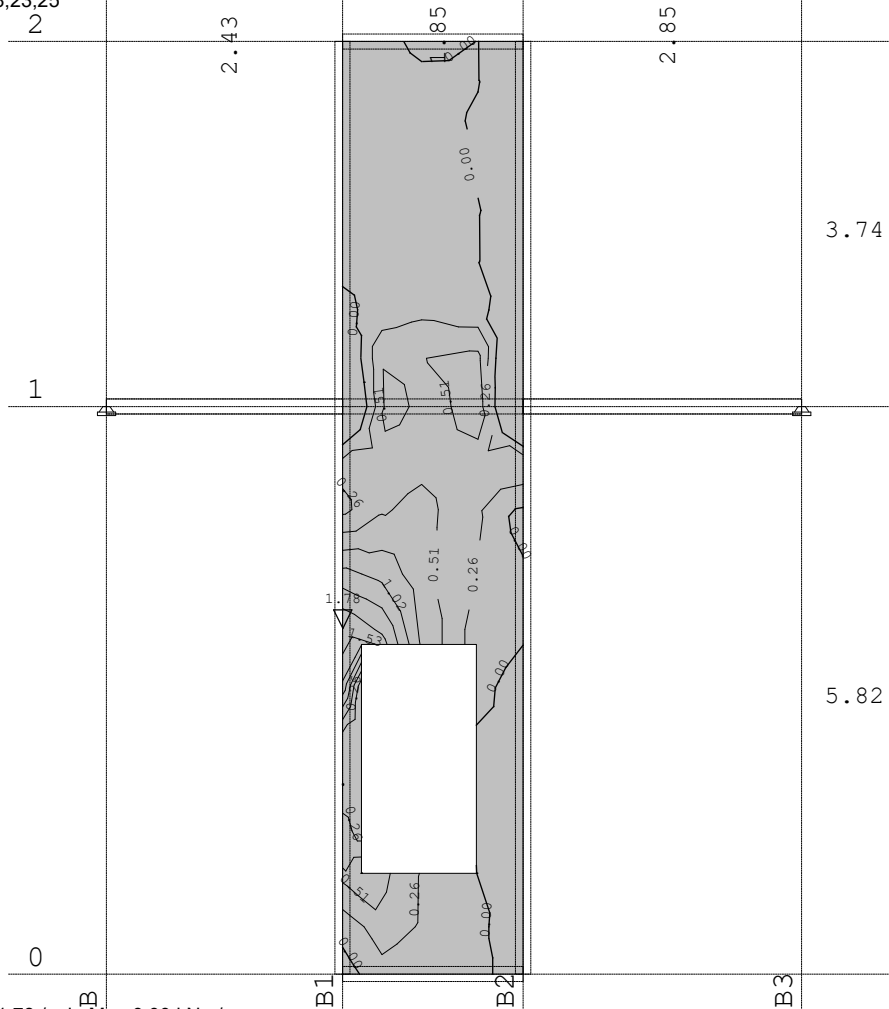
Obt. 31: [Ovo] 5-11,15-18,23,25



Okvir: st Y1

Vplivi v plošči: max  $M_x = 0.00$  / min  $M_x = -1.83$  kNm/m

Obt. 31: [Ovo] 5-11,15-18,23,25

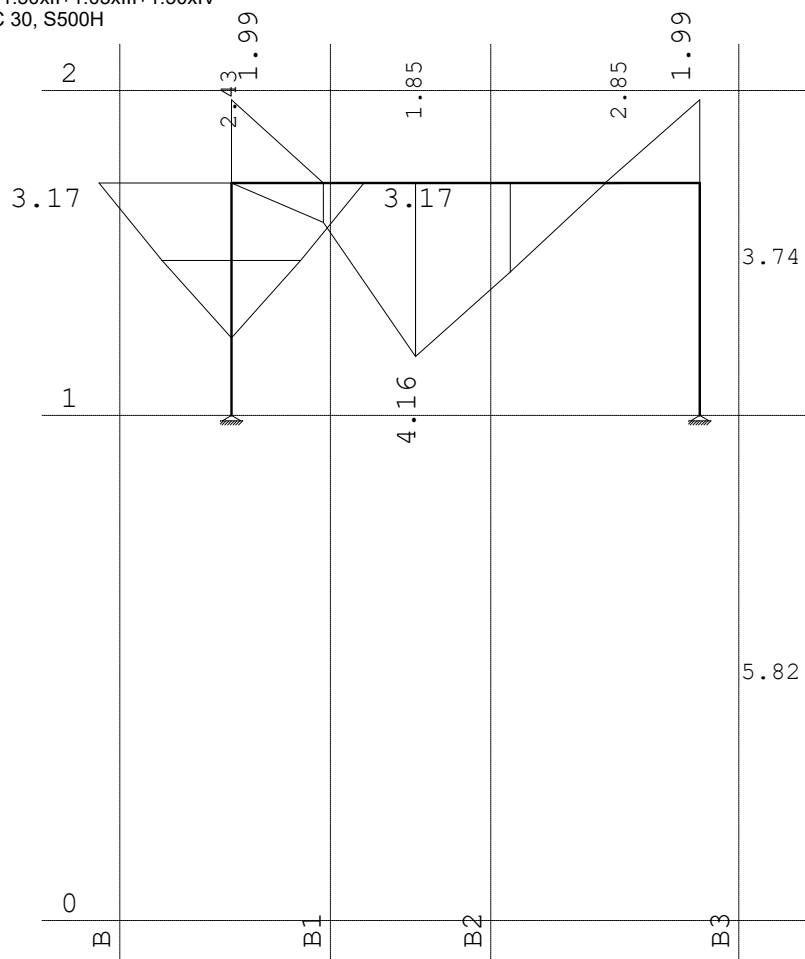


Okvir: st Y1

Vplivi v plošči: max  $M_x = 1.78$  / min  $M_x = 0.00$  kNm/m

**Dimenzioniranje (beton)**

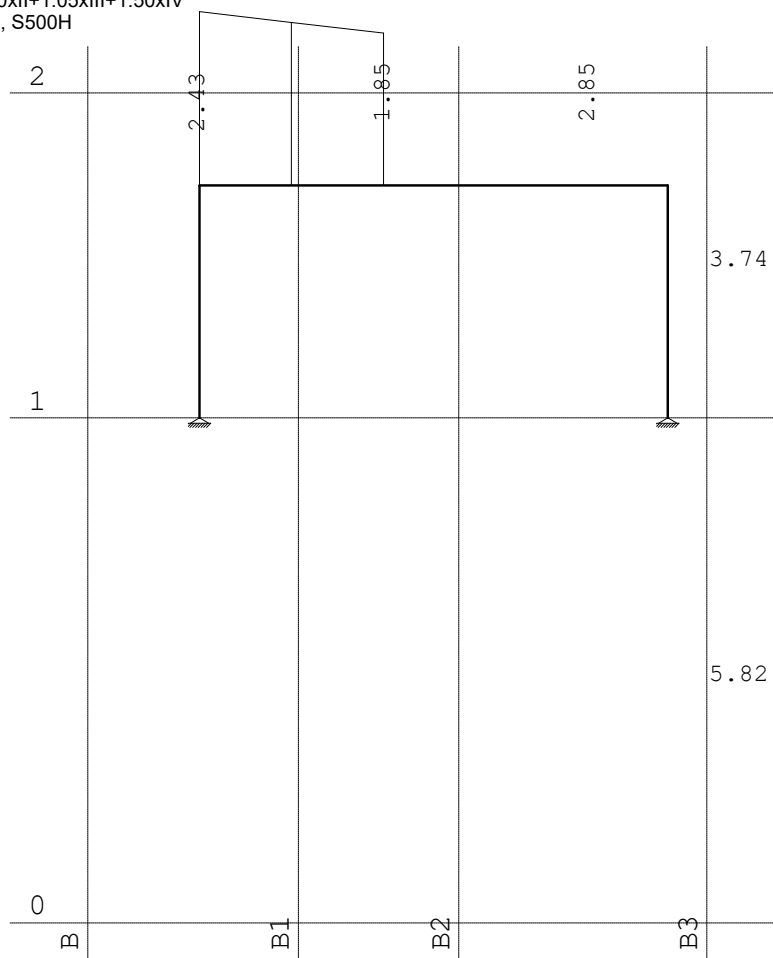
Merodajna obtežba: 1.35xI+1.50xII+1.05xIII+1.50xIV  
 EC 2 (EN 1992-1-1:2004), C 30, S500H



Okvir: st Y2

Armatura v gredah: max  $Aa2/Aa1 = 3.17 / 4.16 \text{ cm}^2$

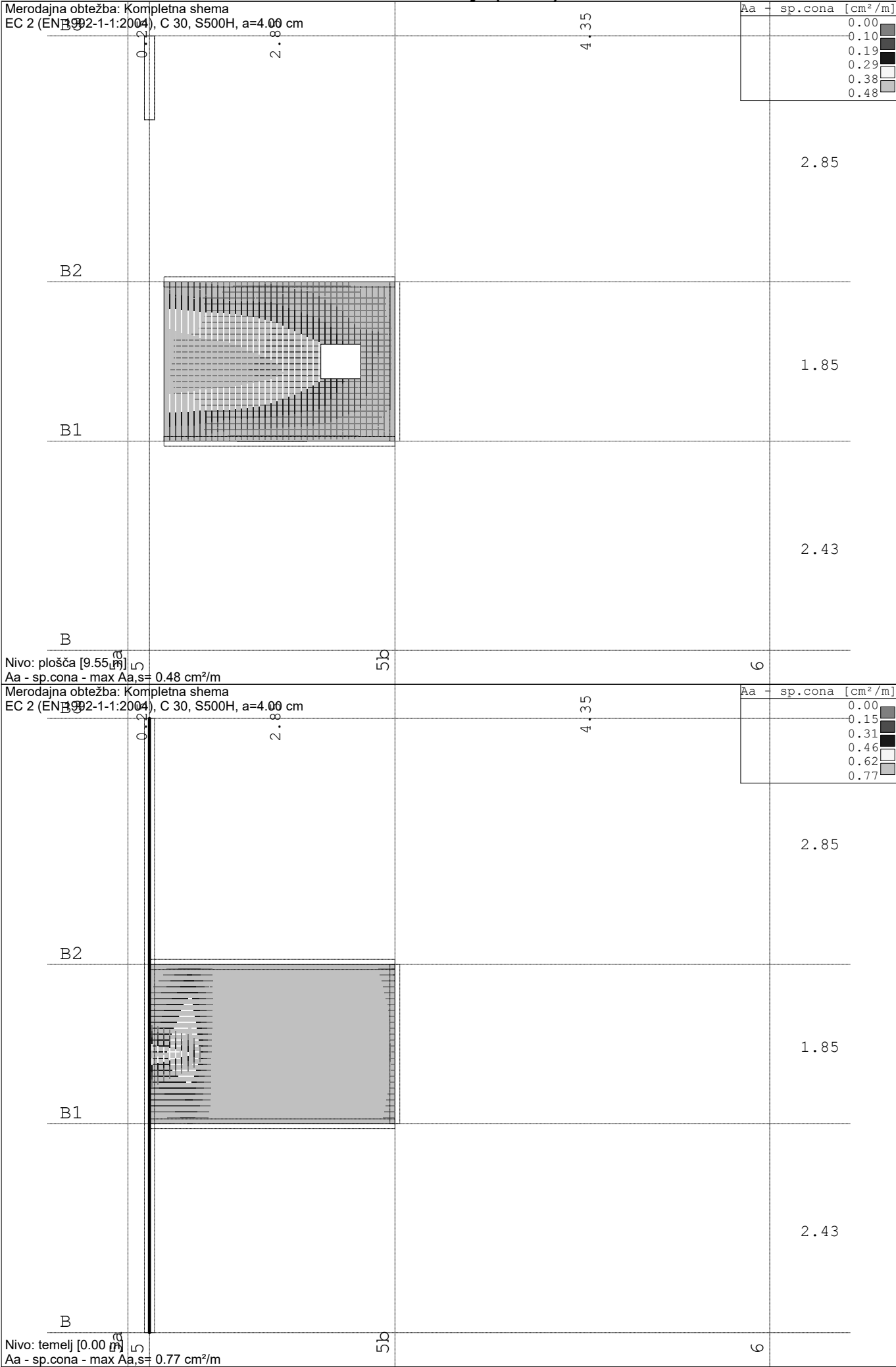
Merodajna obtežba: 1.35xI+1.50xII+1.05xIII+1.50xIV  
 EC 2 (EN 1992-1-1:2004), C 30, S500H



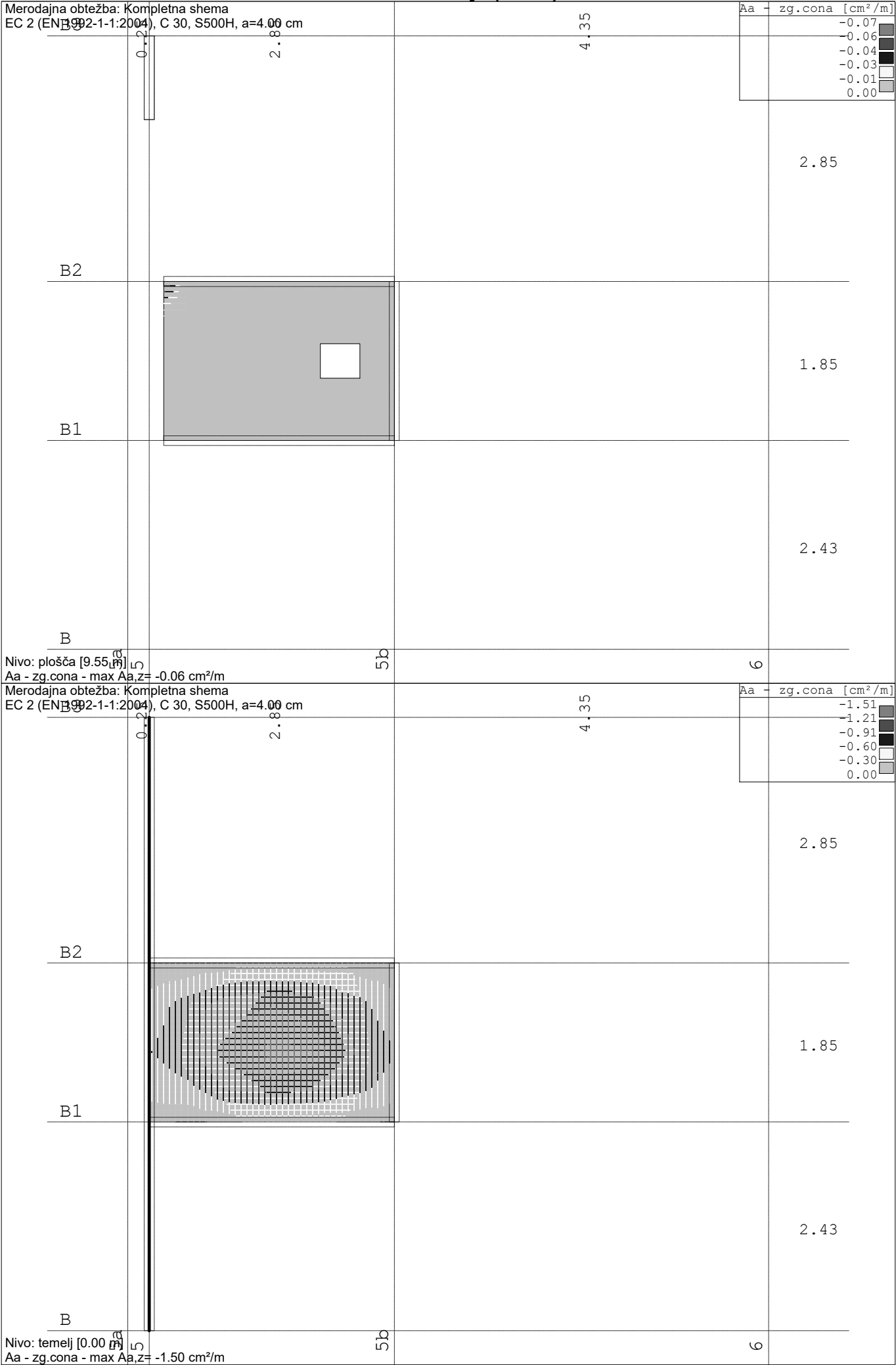
Okvir: st Y2

Armatura v gredah: max  $Aa, st = 1.70 \text{ cm}^2$

Dimenzioniranje (beton)



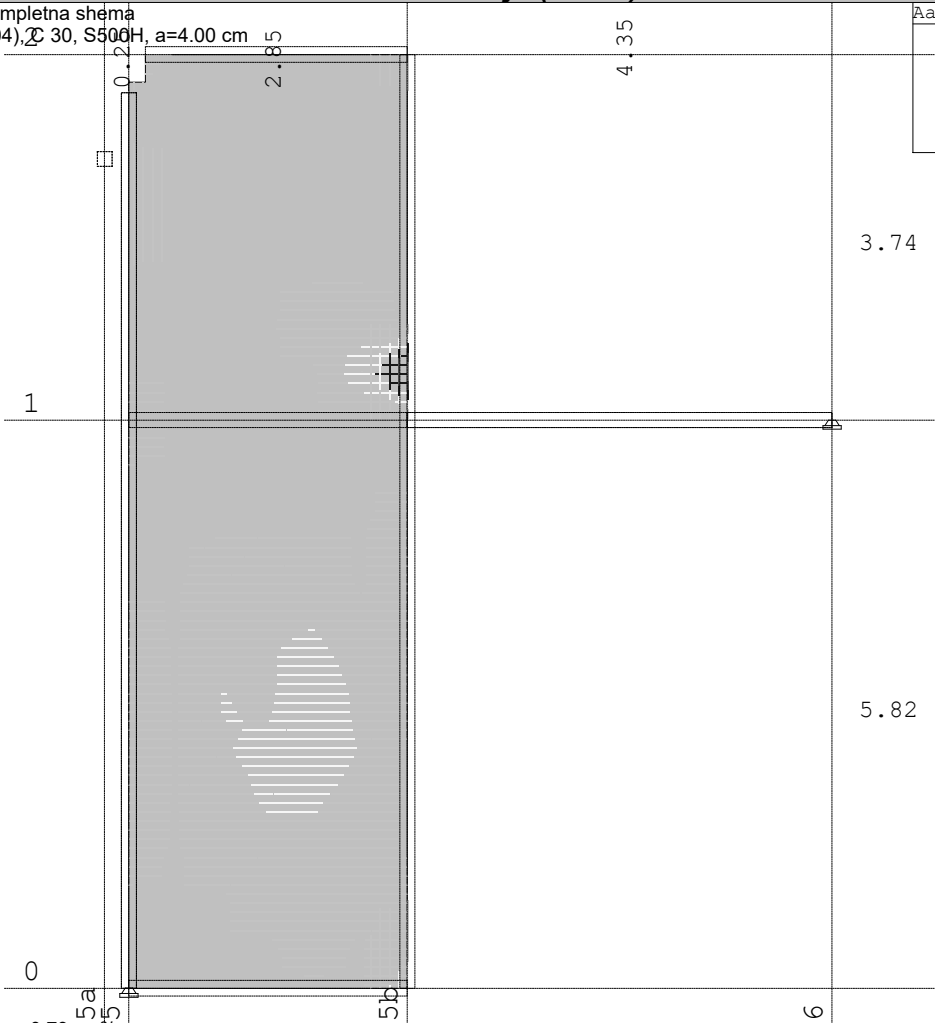
Dimenzioniranje (beton)



Dimenzioniranje (beton)

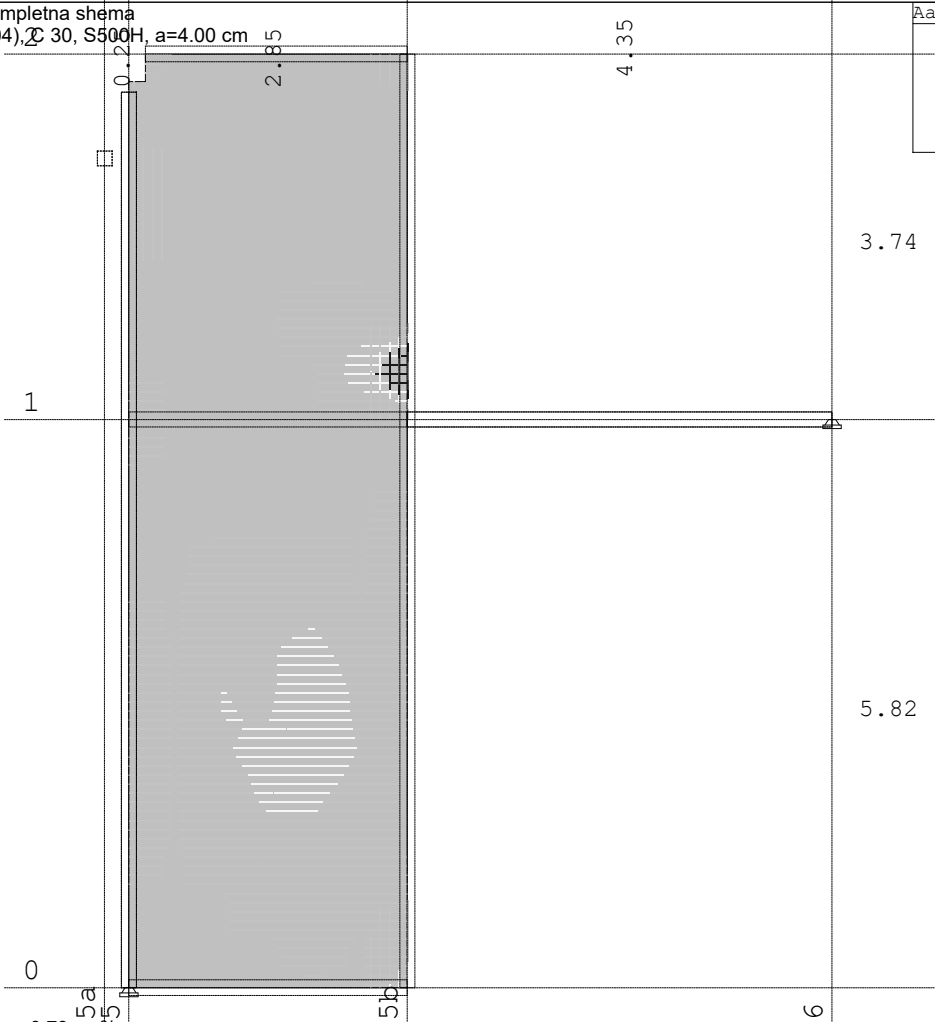
Merodajna obtežba: Kompletna shema  
EC 2 (EN 1992-1-1:2004), C 30, S500H, a=4.00 cm

Aa - zg.cona [cm²/m]	
-0.79	
-0.63	
-0.47	
-0.32	
-0.16	
0.00	



Okvir: st X1  
Aa - zg.cona - max Aa,z= -0.79 cm²/m  
Merodajna obtežba: Kompletna shema  
EC 2 (EN 1992-1-1:2004), C 30, S500H, a=4.00 cm

Aa - zg.cona [cm²/m]	
-0.79	
-0.63	
-0.47	
-0.32	
-0.16	
0.00	



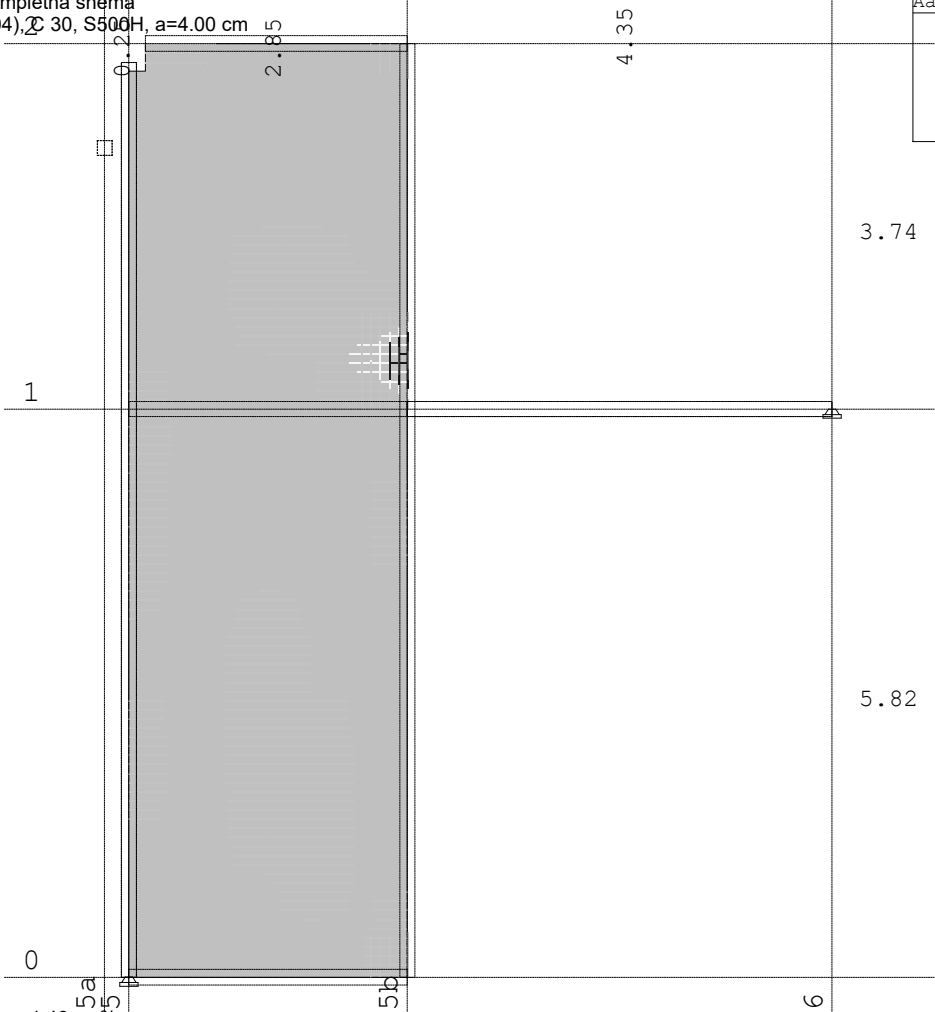
Okvir: st X1  
Aa - zg.cona - max Aa,z= -0.79 cm²/m



Dimenzioniranje (beton)

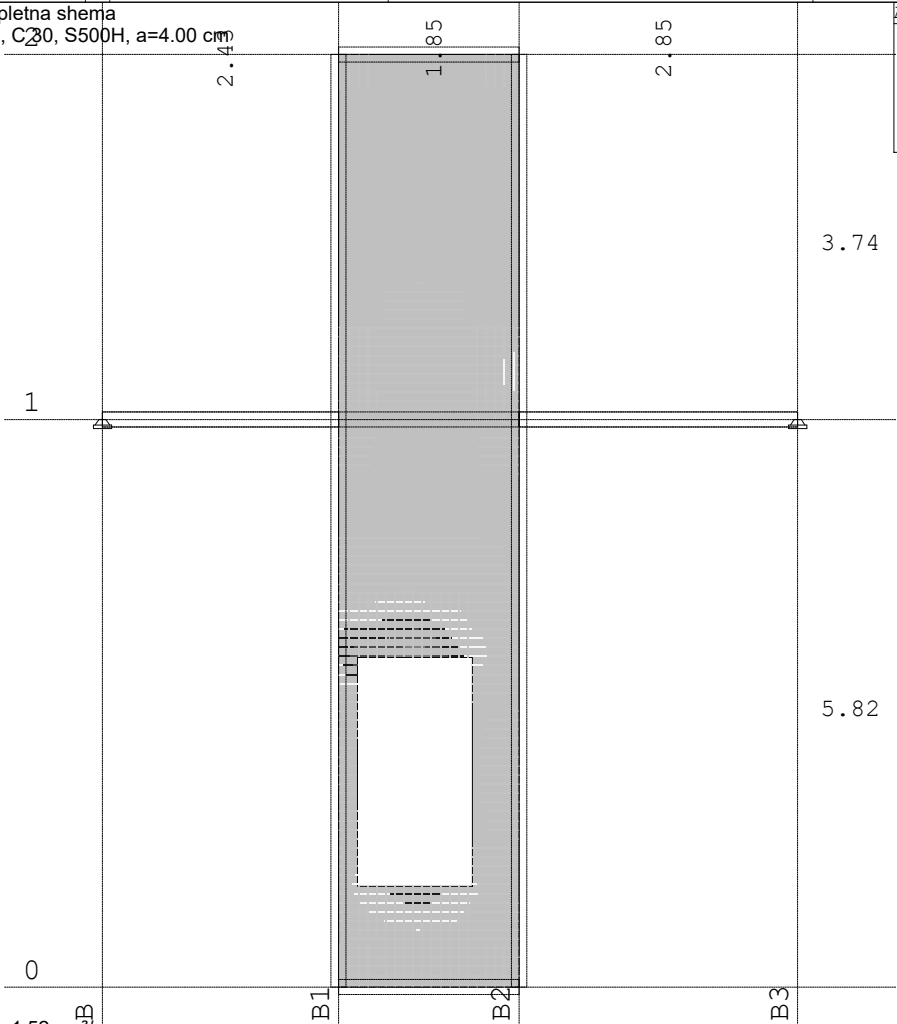
Merodajna obtežba: Kompletna shema  
EC 2 (EN 1992-1-1:2004), C30, S500H, a=4.00 cm

Aa - zg.cona [cm²/m]
-1.46
-1.17
-0.88
-0.58
-0.29
0.00



Okvir: st X2  
Aa - zg.cona - max Aa,z= -1.46 cm²/m  
Merodajna obtežba: Kompletna shema  
EC 2 (EN 1992-1-1:2004), C30, S500H, a=4.00 cm

Aa - zg.cona [cm²/m]
-1.53
-1.22
-0.92
-0.61
-0.31
0.00



Okvir: st Y1  
Aa - zg.cona - max Aa,z= -1.52 cm²/m